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March 6, 2015

RECEIVED

MAR 06 2015

ENVIRONMENTAL HEALTH

Greg McNalley
Lewis & Clark County Planning Department
316 N. Park Avenue Room 230
Helena, MT 59623

**RE: Engineered Fire Suppression System Plans
Heron Creek Subdivision, Phases I - III**

Dear Greg:

Per your request during our meeting on Monday, we have enclosed engineered plans, material specifications, and pump performance curves for the Herron Creek Fire Suppression System. The system shown on these plans will replace much of an existing fire pumping system currently constructed at the site. The existing system was designed by Great West Engineering to produce 1000 GPM @ 20PSI; however testing of the system has resulted in pump cavitation issues and a flow of approximately 500 GPM at the nearest hydrant.

We have attached the original fire system construction plans as well as a 2007 signed agreement with Chief Drake that approved the current system configuration. These documents have been attached only to provide the peer reviewer with a history of the system.

The proposed fire suppression system must satisfy Condition of Final Plat Approval #9 of Phase I:

"The Applicant and the County must agree, prior to final plat approval, on fire protection measures that minimize the risk of fire and that permit the effective and efficient suppression of fires"

The fire protection system proposed consists of the following:

- Fire water storage will consist of an existing, lined, open-water pond; approximately 6 – 8 feet deep with a liquid capacity of approximately 200,000 gallons. The pond will contain the required volume 365 days/year regardless of ice buildup.
- New 10" PVC piping installed level between a self cleaning intake strainer (in the pond) and a new wet well.
- A Clemons® Clearwater self-cleaning suction screen (10" diameter, Model CW1000) will be utilized to mitigate pump intake clogging due to debris. The unit will be pressurized and fed water using the same fire pump that feeds the hydrants and therefore will operate when a pump is activated. The self-cleaning suction screen feed line will also function to "exercise" the fire pump periodically (every 2 weeks); therefore the screen will be cleaned regularly regardless of hydrant flow.
- The wet well will contain one (1) line-shaft vertical turbine pump.

- The pump motor (50 HP, 460v, 3 phase) and soft start controller (pressure activated) will be housed directly atop the wet well in a heated, insulated, and ventilated stick-built structure with concrete foundation.
- The structure will also contain the required pressure tank, transducers, valves, etc.
- The pumping system is setup to be pressure-controlled; however it can also be controlled manually via the control panel.
- The discharge from the fire pump will be conveyed within a new 8" diameter C900 PVC water line to a connection with the existing 6" diameter SCH 40 PVC fire distribution lines.
- The pump control panel will "exercise" the pump regularly to ensure the motor does not seize due to infrequent use. The control panel will also be linked to an exterior warning light that will alert residents of system warnings.
- When the pump is exercised it will also serve to periodically clean the intake screen.
- The pond will continually be refilled as needed by a dedicated 40 GPM well (GWIC #261710). The well will fill the pond when commanded by a pressure transducer located within the wet well. Because the refill piping is located within a heated structure, the refill system will function 365 days/year.
- Per the request of Chief Drake, we have also added a dry hydrant with separate intake strainer to the pond design. The dry hydrant will be available independent of the pumping system and lends redundancy to the system design.

Proposed System Performance:

- 1) The system shall provide a flow of 1000 GPM at a minimum of 20PSI, continuously for a minimum of two hours.
- 2) The system shall contain two (2) hydrants. The hydrants shall be located within 1000' of each home within the Herron Creek Subdivision.

System Maintenance & Funding:

The fire water system shall be maintained without funding from an RID. Responsibility for maintenance and funding for such shall be by the Herron Creek HOA as required within the Declaration of Covenants.

The Declaration of Covenants shall require a joint account be created for the sole purpose of fire system maintenance. Five percent (5%) of the annual HOA dues will be diverted into this account until the balance reaches \$20,000.00. The fund will then be maintained at this amount until maintenance is needed. The five percent (5%) contribution shall resume each time the account balance falls below \$20,000.00. The covenants will be written so that the future HOA cannot vote the fire suppression funding mechanism out.

Easements will be recorded on the final plat to ensure the fire pumping system, pond, piping, and all related appurtenances can be maintained and/or replaced when needed.

System Testing:

The completed system will be tested to ensure it can reliably supply 1000 GPM for two hours @ 20 PSI to the hydrants. Testing will be conducted jointly by the Tri-Lakes VFD and Casne & Associates. Flow measurements will be made at the furthest hydrant from the pumping system.

Please feel free to call if you have any questions.

Sincerely,
CASNE & ASSOCIATES, INC



By: Ryan E. Casne, P.E.
Senior Engineer, Principal

C.C.: Ron Bartsch, Owner, Sussex Development
File

Enclosed: Current Fire System Plans (2)

PROPOSED FIRE SYSTEM PLANS

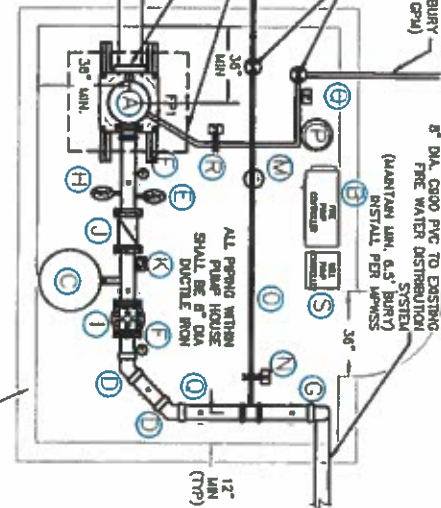
2" PVC FROM FIRE WELL
6.5' MIN BURY
(40 GPM)

FLOOR PENETRATION AND PVC
SLEEVE

PROVIDE ROOF HATCH FOR
PUMP SERVICE AND REMOVAL
10"x16" TIE IN WET WELL
(SEE CROSS SECTION)

10" DIA. C900 PVC PIPE
INSTALLED LEVEL BETWEEN WET
WELL AND POND INTAKE
STRAINER

HEATED, INSULATED, AND VENTED
CONTROLS BUILDING W/
ROOF HATCH FOR PUMP REMOVAL



PLUMBING LEGEND

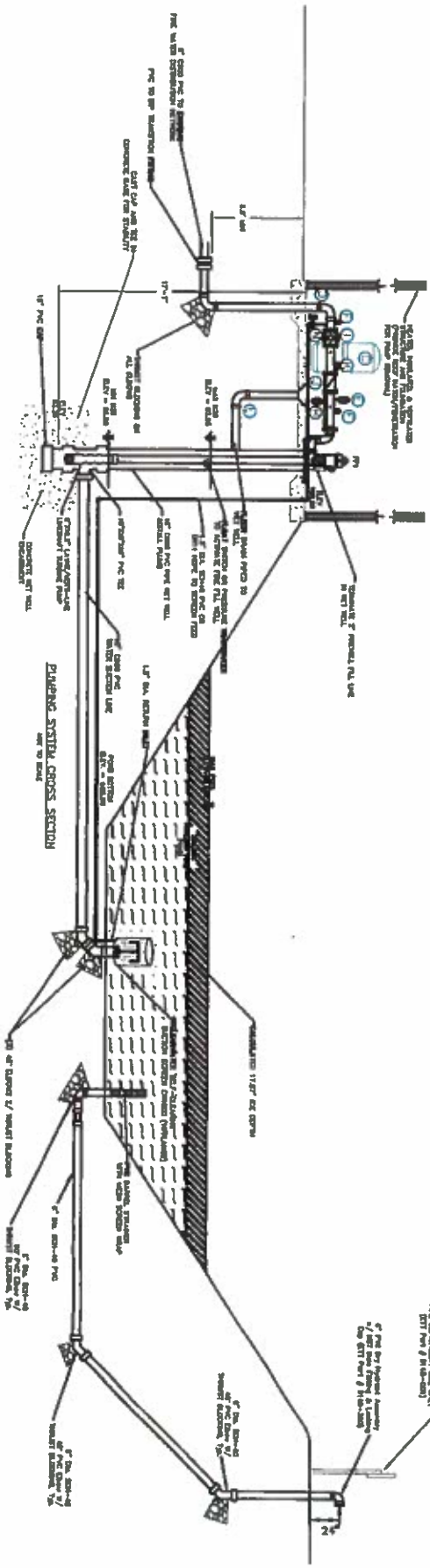
- A SEE PUMP SCHEDULE
- B PUMP CONTROLLER
- C CROCO MP-5540 -50HP W/ SFT MOTOR START
- D WELL-X-TROL W/CSO HYDRO-PNEUMATIC PRESSURE TANK
- E 45' DRP ELBOW W/ MECHANICAL RESTRAINTS
- F 1" AIR RELIEF VALVE - CRISPEN OR APPROVED EQUAL
- G 0-200 PSIG PRESSURE GAUGE
- H 90° DRP ELBOW W/ MECHANICAL RESTRAINTS
- I 1" PRESSURE RELIEF VALVE (SET AT 100PSI); DISCHARGE
PED TO WET WELL OR BUILDING EXTERIOR
- J 6" RESILIENT WEDGE GATE VALVE (MELLER OR EQUAL)
- K 6" SWING CHECK VALVE: KENNEDY OR EQUAL
- L PRESSURE TRANSDUCER (PER CONTROL PANEL
MANUFACTURER'S REC.)
- M 6" DIA. FLOOR DRAIN PED TO WET WELL
- N PRESTANDARD & RESTRAINT 1", BOLT TO FLOOR W/ (4)
DRILLED ANCHOR BOLTS, 2 HEX BOLTS, & LOCK WASHERS.
- O 1-1/2" BUTTERFLY VALVE W/ SOLENOID (FOR BYPASS PUMPING
TO PUMP SCREEN INLET)
- P 1-1/2" SCH40 PVC OR DR11 HOLE LINE FROM BUTTERFLY
VALVE TO SELF-CLEANING INTAKE SCREEN (6.5' MIN BURY)
- Q W/CSO HYDRO-PNEUMATIC PRESSURE TANK
- R PRESSURE SWITCH
- S 2" BUTTERFLY VALVE W/ SOLENOID (FOR FIREWELL RETUL)
- T FLOAT/TRANSDUCER ACTIVATED WELL PUMP CONTROLLER

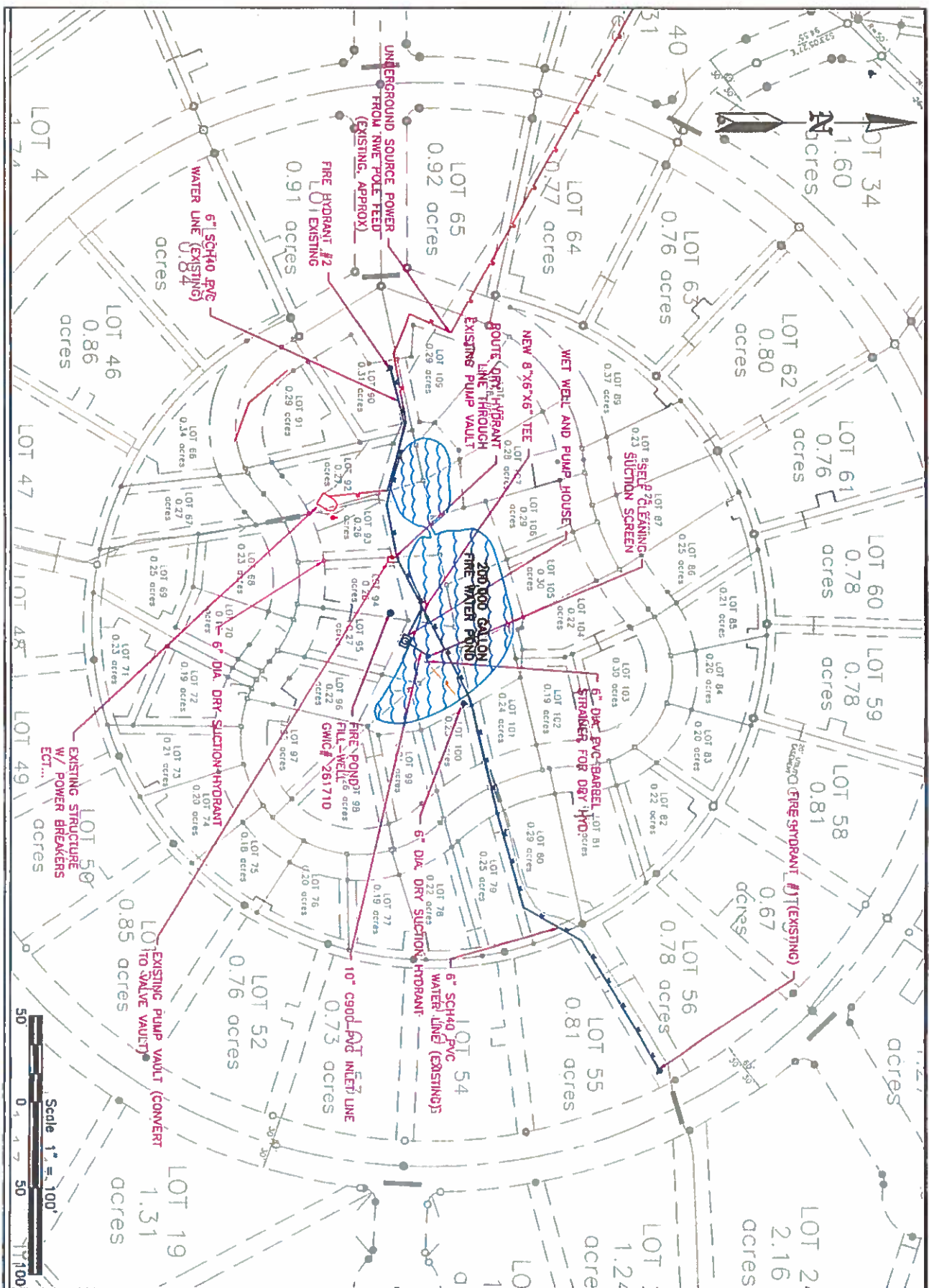
GENERAL SPECIFICATIONS & CONSTRUCTION NOTES:

1. ALL WORK TO BE PERFORMED FOR THE INSTALLATION OF THE FIRE WATER SUPPRESSION SYSTEM SHALL BE IN ACCORDANCE WITH ALL APPLICABLE ELECTRICAL AND COMMERCIAL PLUMBING CODES.
2. ALL MATERIALS USED SHALL BE NSF OR AWWA APPROVED. A FULL MATERIALS SUBMITTAL PACKAGE IS REQUIRED PRIOR TO PROCEEDING WITH THE WORK.
3. PLUMBER SHALL PROVIDE ENGINEER WITH AS-BUILT DRAWINGS UPON COMPLETION OF INSTALLATION.
4. PLUMBER SHALL PROVIDE ENGINEER WITH MANUFACTURER'S DATA SHEETS, WARRANTY SLIPS, OWNER'S MANUALS, ETC. FOR ALL EQUIPMENT INSTALLED.

FIRE PUMP SCHEDULE

QNT	TYPE	QTY	DN	80PSI	1P	PUMP	PUMP	ELECTRICAL
						START	STOP	V
						(P/S)	(P/S)	PH
								HE
P-1	DIAPHRAGM PUMP	1000	150 (15 FT)	1600	30	30	440	3
	W/CSO LINE/NOISE							BO





EXISTING SYSTEM CONSTRUCTION PLANS (BY OTHERS)



May 9, 2007

Bob Drake
Tri-Lakes Volunteer Fire Department
3200 Spokane Creek Road
East Helena, MT 59635

COPY

RE: Fire Protection Plan, Heron Creek Subdivision

Dear Mr. Drake:

Thank you for meeting with us last Tuesday to discuss the many options for fire mitigation at the proposed Heron Creek Subdivision. Please consider this letter a proposed "Fire Protection Plan". Below is a list of the preferred and agreed upon mitigation measures for the proposed Heron Creek Subdivision.

1. The owner will install two fire hydrants capable of flowing 1,000 gallons per minute for a period of two hours at a minimum pressure of 20 psi. One of the hydrants will be located at the parking area near the entrance to the condominium/multi family unit lot in the center of the proposed development. The second hydrant will be located on the east side of Fire Weed Street near where the trail/emergency access, creek crosses. As a result of the placement of these two hydrants and the emergency access provisions, there will be a hydrant within 1000 ft of all structures.
2. Roadways and parking areas will be designed to help ensure emergency access to fire hydrants.
3. The water storage will be supplied with adequate capacity to provide the required 1,000 gallons per minute fire flow for a period of two hours year around. Make up water will be supplied through a combination of sources and controlled by pressure transducers or other acceptable controls ensuring adequate capacity year around. The water structure will operate year around, which will reduce the amount of ice buildup by keeping the water moving. The storage will be sized with consideration of reasonable ice buildup. The storage level will be controlled via subsurface controls so they will work during cold weather. It is likely that the majority of the ponds and stream will be shut down during the winter months. The water feature used for fire storage will continue to operate and makeup water will be supplied by a well drilled for fire protection. This project anticipates full time maintenance personnel for the community, therefore helping to ensure the fire fill station remain in good operational condition.
4. We discussed the challenges related to using ponds to store and supply the water for



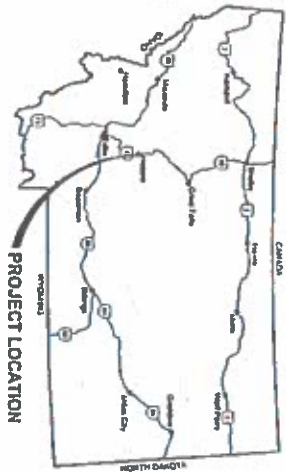
fire protection. In order to mitigate some of these challenges, the water feature supplying the fire water will be designed to minimize silting of the water storage capacity. This will be accomplished through a combination of settling basins and possibly other technologies prior to the water entering the storage area.

5. By providing the two hydrants within 1,000 feet of the condominiums, the emergency access route at the east side of the condominium units, providing "no parking signs", the off-street parking pads in front of each garage, and designating one way traffic, the reduced driving surface width within the condominium lot will be acceptable to the fire department. As a result of all these provisions, the fire department will be able to easily reach the condominiums with hose lays and not have to tanker-shuttle water on this interior road.
6. Removable bollards will be provided for the emergency access route on the east side of the condominium lot between lot #55 and lot #56, and the access to the drain field area located between lot #1 and lot #2.
7. As part of the maintenance of the community and in compliance with the proposed Vegetation Management Plan, the parks and wastewater facility areas will be maintained as parkland. The grasses will be mowed and trees maintained. All lots will be required to maintain mowed grass or landscaping on the entire lot. Specific details will be worked out with the fire chief and included in the covenants.

This letter of understanding covers the major issues discussed in the meeting. This letter does not limit additional measures or safeguards to be negotiated between Tri-Lakes Volunteer Fire Department and the owner.


Ron Bartsch, Owner


Bob Drake, Fire Chief



FIREFLOW SYSTEM **HERON CREEK SUBDIVISION** **CONSTRUCTION PLANS**

SECTION 12, TOWNSHIP 10N, AND RANGE 2W



NOT TO SCALE

SHEET INDEX

SHEET 1 COVER
 SHEET 2 LEGEND-NOTES-ABBREVIATIONS
 SHEET 3 SITE PLAN
 SHEET 4 DETAILS

PROJECT 148179
 DATE 08/04/2011

PLANS PREPARED FOR:
 HERON CREEK SUBDIVISION

APPROVED BY:

SHAWN BRYANT, P.E.
 GREAT WEST ENGINEERING



QA/QC BY:

NAME, P.E.
 GREAT WEST ENGINEERING

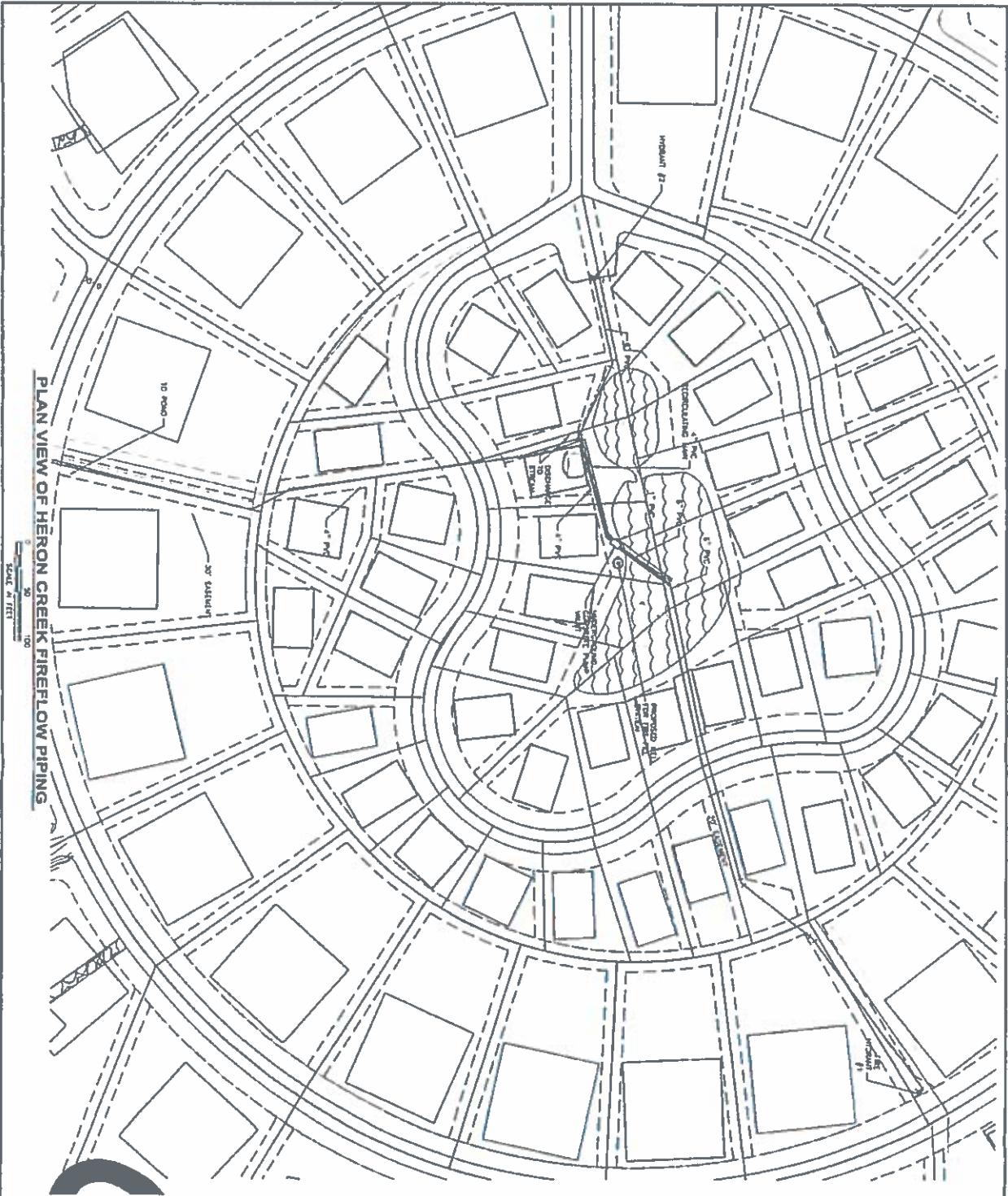
PLANS PREPARED BY:
 CARRE CAUCHER



NO.	REVISION	DATE	BY	CHKD.
1				
2				
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ABBREVIATIONS

SYMBOL	ABBREVIATION	DESCRIPTION
1	1"	1" DIA. PIPE
2	2"	2" DIA. PIPE
3	3"	3" DIA. PIPE
4	4"	4" DIA. PIPE
5	5"	5" DIA. PIPE
6	6"	6" DIA. PIPE
7	8"	8" DIA. PIPE
8	10"	10" DIA. PIPE
9	12"	12" DIA. PIPE
10	14"	14" DIA. PIPE
11	16"	16" DIA. PIPE
12	18"	18" DIA. PIPE
13	20"	20" DIA. PIPE
14	24"	24" DIA. PIPE
15	30"	30" DIA. PIPE
16	36"	36" DIA. PIPE
17	42"	42" DIA. PIPE
18	48"	48" DIA. PIPE
19	54"	54" DIA. PIPE
20	60"	60" DIA. PIPE
21	66"	66" DIA. PIPE
22	72"	72" DIA. PIPE
23	78"	78" DIA. PIPE
24	84"	84" DIA. PIPE
25	90"	90" DIA. PIPE
26	96"	96" DIA. PIPE
27	102"	102" DIA. PIPE
28	108"	108" DIA. PIPE
29	114"	114" DIA. PIPE
30	120"	120" DIA. PIPE
31	126"	126" DIA. PIPE
32	132"	132" DIA. PIPE
33	138"	138" DIA. PIPE
34	144"	144" DIA. PIPE
35	150"	150" DIA. PIPE
36	156"	156" DIA. PIPE
37	162"	162" DIA. PIPE
38	168"	168" DIA. PIPE
39	174"	174" DIA. PIPE
40	180"	180" DIA. PIPE
41	186"	186" DIA. PIPE
42	192"	192" DIA. PIPE
43	198"	198" DIA. PIPE
44	204"	204" DIA. PIPE
45	210"	210" DIA. PIPE
46	216"	216" DIA. PIPE
47	222"	222" DIA. PIPE
48	228"	228" DIA. PIPE
49	234"	234" DIA. PIPE
50	240"	240" DIA. PIPE
51	246"	246" DIA. PIPE
52	252"	252" DIA. PIPE
53	258"	258" DIA. PIPE
54	264"	264" DIA. PIPE
55	270"	270" DIA. PIPE
56	276"	276" DIA. PIPE
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288	1668"	1668" DIA. PIPE
289	1674"	1674" DIA. PIPE
290	1680"	1680" DIA. PIPE
291	1686"	1686" DIA. PIPE
292	1692"	1692" DIA. PIPE
293	1698"	1698" DIA. PIPE
294	1704"	1704" DIA. PIPE
295	1710"	1710" DIA. PIPE
296	1716"	1716" DIA. PIPE
297	1722"	1722" DIA. PIPE
298	1728"	1728" DIA. PIPE
299	1734"	1734" DIA. PIPE
300	1740"	1740" DIA. PIPE
301	1746"	1746" DIA. PIPE
302	1752"	1752" DIA. PIPE
303	1758"	1758" DIA. PIPE
304	1764"	1764" DIA. PIPE
305	1770"	1770" DIA. PIPE
306	1776"	1776" DIA. PIPE
307	1782"	1782" DIA. PIPE
308	1788"	1788" DIA. PIPE
309	1794"	1794" DIA. PIPE
310	1800"	1800" DIA. PIPE
311	1806"	1806" DIA. PIPE
312	1812"	1812" DIA. PIPE
313	1818"	1818" DIA. PIPE
314	1824"	1824" DIA. PIPE
315	1830"	1830" DIA. PIPE
316	1836"	1836" DIA. PIPE
317	1842"	1842" DIA. PIPE
318	1848"	1848" DIA. PIPE
319	1854"	1854" DIA. PIPE
320	1860"	1860" DIA. PIPE
321	1866"	1866" DIA. PIPE
322	1872"	1872" DIA. PIPE
323	1878"	1878" DIA. PIPE
324	1884"	1884" DIA. PIPE
325	1890"	1890" DIA. PIPE
326	1896"	1896" DIA. PIPE
327	1902"	1902" DIA. PIPE
328	1908"	1908" DIA. PIPE
329	1914"	1914" DIA. PIPE
330	1920"	1920" DIA. PIPE
331	1926"	1926" DIA. PIPE
332	1932"	1932" DIA. PIPE
333	1938"	1938" DIA. PIPE
334	1944"	1944" DIA. PIPE
335	1950"	1950" DIA. PIPE
336	1956"	1956" DIA. PIPE
337	1962"	1962" DIA. PIPE
338	1968"	1968" DIA. PIPE
339	1974"	1974" DIA. PIPE
340	1980"	1980" DIA. PIPE
341	1986"	1986" DIA. PIPE
342	1992"	1992" DIA. PIPE
343	1998"	1998" DIA. PIPE
344	2004"	2004" DIA. PIPE
345	2010"	2010" DIA. PIPE
346	2016"	2016" DIA. PIPE
347	2022"	2022" DIA. PIPE
348	2028"	2028" DIA. PIPE
349	2034"	2034" DIA. PIPE
350	2040"	2040" DIA. PIPE
351	2046"	2046" DIA. PIPE
352	2052"	2052" DIA. PIPE
353	2058"	2058" DIA. PIPE
354	2064"	2064



PLAN VIEW OF HERON CREEK FIREFLOW PIPING

SCALE: 1\"/>

NOTE:
ALL BLOCKS ARE FOR INFORMATION PURPOSES
AND SHOULD NOT BE USED FOR BLOCKING A
BLOCK



3
OF 4

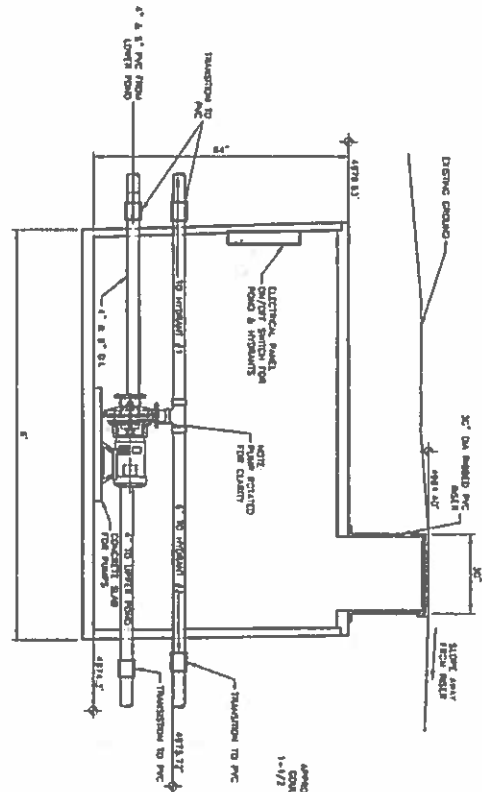
FIREFLOW SYSTEM
HERON CREEK SUBDIVISION

SITE PLAN

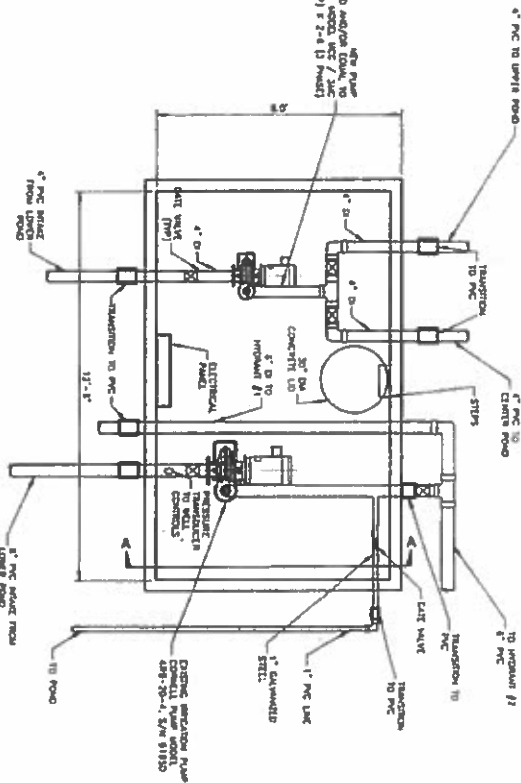


PROJECT	NO.	REVISION DESCRIPTION	BY	DATE
DESIGNED CAD	1			
DRAWN CAD	2			
CHECKED KB	3			
APPROVED	4			
DATE: MARCH 2001				

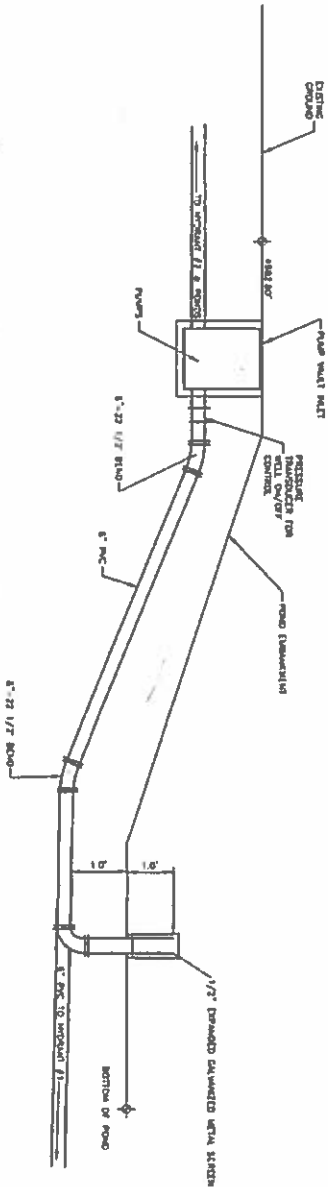
PROFILE VIEW OF PUMP VAULT A-A



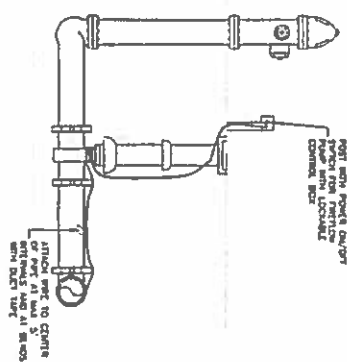
PLAN VIEW OF PUMP VAULT



7 PROFILE DETAIL OF POND PIPING EMBANKMENT



HYDRANT POWER DETAIL



PUMPING SYSTEM MATERIALS



Advanced Pump & Equipment

1408 Gold Ave Ste 6, Bozeman, MT 59718

Phone 406-586-1700 Fax 406-586-1710

orders@advpump.com

QUOTE

QUOTE #

AAAQ1646

DATE

Mar 24, 2014

To

Ship To

Phone

SALESPERSON	P.O. Number	PAYMENT TERMS	DUE DATE
		50% deposit / 50 % at shipment	

QTY	MPN	DESCRIPTION	UNIT PRICE	TOTAL PRICE
1		10THC Layne/ Verti-Line Lineshaft Turbine		
		8" x 16 1/2" Layne / Verti-Line Water Lube Discharge Head		
		-1-3/16" Packing Box		
		-8" x 1 3/16" x Length Needed Water Lube T&C Column Complete w/ 5' Bearings Spacing		
		-4 Stage 10THC Layne/ Verti-Line W/L Bowl Assembly		
		-Cast-Iron Bronze Fitted: 8" x 1 3/16" x Bell		
		-Standard shop coat enamel paint		
		-16" ID x 176" Deep Casing Required***		
		-30" Submergence Over Bell Lip Required***		
		Removable Steel Sole Plate (1" Thick)		
		Galvanized Steel Basket Strainer		
		50 HP USEM VHS Motor w/ 1 3/16" NRR 3/60/460/WP-1 Type RU Standard Eff		
		Orenco Control Panel MVP-S460 3Ø CV RVSS TR 50HP		
		Panel Includes:		
		• NEMA 3R Steel Wall-Mount Enclosure		
		• Enclosure Heater & Fan		
		• Orenco MVP (Logo) Controller		
		• Programmed As Required Per Functional Description Provided		
		• Soft Starter w/ Overload For One 460VAC 50HP Pump		
		• Isolation & Shorting Contactors		
		• Motor Circuit Breaker, 100A		
		• Control Transformer With Primary Fusing, 350VA, 460-115V		
		• Controls Circuit Breaker		
		• Valve Circuit Breaker (115VAC valve)		
		• HOA Switches (one for pump, one for valve)		
		• General Alarm Beacon Light (loose for site installation by others)		
		• Terminal Blocks as required		
		• Input For Up To Two Pressure Switches		
		• Control Relays As Required		
		• Remote Alarm Contact		
		• Labeling & Documentation		
		• UL508a Listed		
		Freight		

Company: Advanced Pump & Equipment

Name:

Date: 2/25/2014



AURORA LAYNE VERTI-LINE SERIES

Pump:

Size: 10THC (4 stage)
 Type: Vertical Turbine
 Synch speed: 1800 rpm
 Curve:
 Specific Speeds:
 Dimensions:
 Vertical Turbine:
 Speed: 1750 rpm
 Dia: 7.98 in
 Impeller:
 Ns: —
 Nss: —
 Suction: 8 in
 Discharge: —
 Bowl size: 9.88 in
 Max lateral: —
 Thrust K factor: 10 lb/ft

Search Criteria:

Flow: 1000 US gpm Head: 136 ft

Fluid:

Water
 Density: 62.32 lb/ft³
 Viscosity: 0.9946 cP
 Temperature: 68 °F
 Vapor pressure: 0.3391 psi a
 Atm pressure: 14.7 psi a
 NPSHa: —

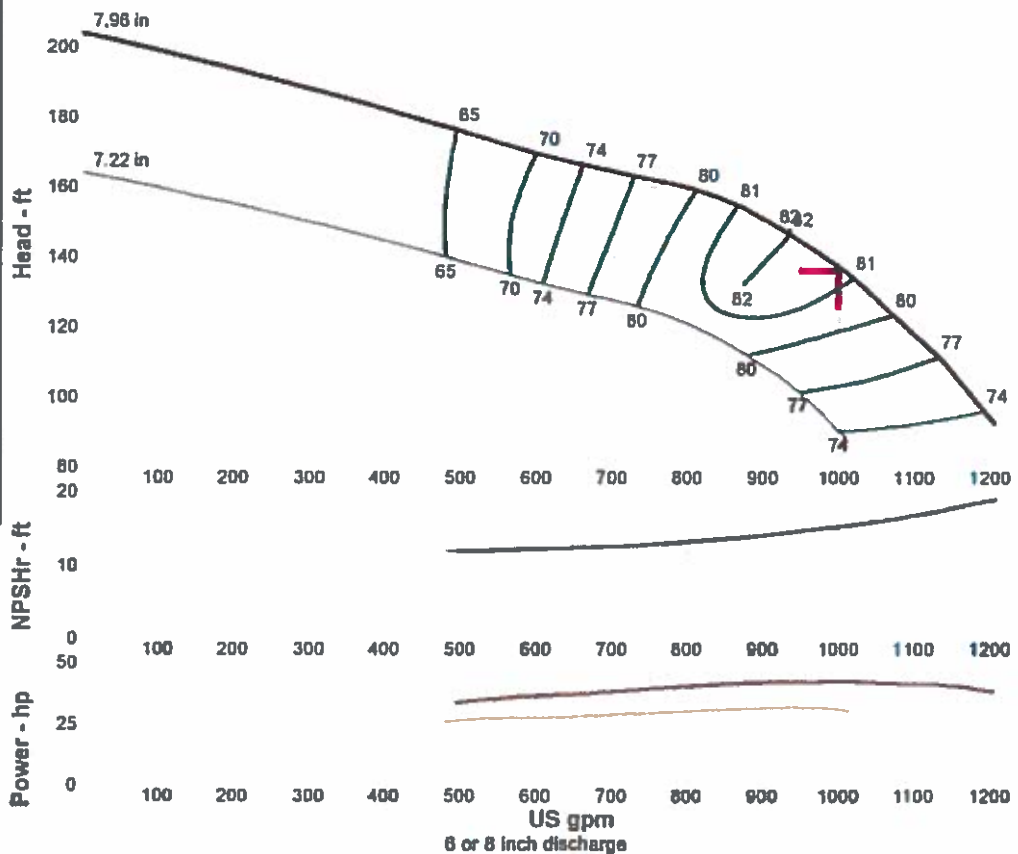
Motor:

Standard: NEMA
 Enclosure: TEFC
 Size: 50 hp
 Speed: 1800
 Frame: 326T
 Sizing criteria: Max Power on Design Curve

Pump Limits:

Temperature: 150 °F
 Pressure: 450 psi g
 Sphere size: 0.94 in
 Power: —
 Eye area: 16.5 in²

Data Point	
Flow:	1000 US gpm
Head:	137 ft
Eff:	81.2%
Power:	42.5 hp
NPSHr:	15.4 ft
Design Curve	
Shutoff head:	204 ft
Shutoff dP:	88.3 psi
Min flow:	—
BEP:	82% @ 935 US gpm
NOL power:	42.6 hp @ 1019 US gpm
Max Curve	
Max power:	42.6 hp @ 1019 US gpm



Performance Evaluation:

Flow US gpm	Speed rpm	Head ft	Efficiency %	Power hp	NPSHr ft
1200	1750	94.2	73.7	38.7	18.9
1000	1750	137	81.2	42.5	15.4
800	1750	160	79.6	40.5	13.3
600	1750	170	70.1	36.7	12.3
400	1750	—	—	—	—

SUCTION CAN SELECTION CHART

Layne/Verti-Line Model	Column Size	Flange O.D.	Max. Bowl O.D.	Clearance (A)	Allowable Capacity (GPM) at a Velocity of 5 Ft./Sec.										
					Can O.D. (D1)										
					8.625	10.75	12.75	14	16	18	20	24	30	36	42
6DRELC	4	6.63	5.63	4			1250								
6DRMC	4	6.63	5.63	4			1250								
6RKLC	4	6.63	5.63	4			1250								
6RKHC	4	6.63	5.63	4			1250								
6EM	4	6.63	5.50	3			1250								
6GM	4	6.63	5.50	4			1250								
6GH	4	6.63	5.50	4			1250								
7EM	4	6.63	6.60	3			1250								
7CL	6	9.25	7.50	3.75				1100							
7CM	6	9.25	7.50	3.75				1100							
7CEH	6	9.25	7.50	3.75				1100							
8URHC	4	6.63	7.75	4.5				1400							
	5	7.63	7.75	4.5				1400							
	6	9.25	7.75	4.5				1100							
8RL	6	9.25	9.50	5					1740						
8RM	6	9.25	9.50	5					1740						
8RH	6	9.25	9.50	5					1740						
8EM	4	6.63	8.00	6				1360							
	6	9.25	8.00	6				1100	1790						
8TM	6	9.25	7.50	4.5				1100	1790						
8TH	6	9.25	7.50	4.5				1100	1790						
10RKLC	5	7.63	9.63	5.5					1700						
	6	9.25	9.63	5.5					1700						
	8	11.75	9.63	5.5					1150						
10RKHC	6	9.25	9.63	5.5					1700						
	8	11.75	9.63	5.5					1150	1950					
10RKEH	6	9.25	9.63	5.5					1700						
	8	11.75	9.63	5.5					1150	1950					
10RKHS	6	9.25	9.63	5.5					1700						
	8	11.75	9.63	5.5					1150						
10EM	4	6.63	10.00	7					1600						
	6	9.25	10.00	7					1600						
10TLC	6	9.25	9.75	5					1680						
	8	11.75	9.75	5					1150	1950					
10THC	6	9.25	9.75	5					1680						
	8	11.75	9.75	5					1150	1950					
10FHM	8	11.75	11.50	7						1950					
10FHH	8	11.75	11.50	7						1950					
11EM	6	9.25	11.38	7						2050					
	8	11.75	11.38	7						1950					
11EH	6	9.25	11.48	7						2000					
	8	11.75	11.48	7						1950					
12RKBL	6	9.25	11.50	6.25						2000					
	8	11.75	11.50	6.25						1950					
	10	13.88	11.50	6.25						1275	2175				
12RKBM	8	11.75	11.75	6.25						1950					
	10	13.88	11.75	6.25						1275	2175				
12RKBH	8	11.75	11.75	6.25						1950					
	10	13.88	11.75	6.25						1275	2175				
12RKBEH	8	11.75	11.75	6.25						1950					
	10	13.88	11.75	6.25						1275	2175				
12TLC	8	11.75	11.75	5.75						1950					
	10	13.88	11.75	5.75						1275	2175				

SUCTION CAN SELECTION CHART

Layne/ Verti-Line Model	Column Size	Flange O.D.	Max. Bowl O.D.	Clearance (A)	Allowable Capacity (GPM) at a Velocity of 5 Ft./Sec.										
					Can O.D. (D1)										
					8.625	10.75	12.75	14	16	18	20	24	30	36	42
12THC	8	11.75	11.75	5.75						1950	2800				
	10	13.88	11.75	5.75						1275	2175	4250			
12EM	6	9.25	13.00	8							2450				
	8	11.75	13.00	8							2450				
12RL	8	11.75	13.00	6.5							2450				
	10	13.88	13.00	6.5							2175				
12RM	8	11.75	13.00	6.5							2450				
	10	13.88	13.00	6.5							2175				
12RH	8	11.75	13.00	6.5							2450				
	10	13.88	13.00	6.5							2175				
12FHL	8	11.75	13.00	7							2450				
	10	13.88	13.00	7							2175				
	12	16.38	13.00	7							1250	3330			
	8	11.75	13.00	7							2450	4500			
12FHM	10	13.88	13.00	7							2175	4250			
	12	16.38	13.00	7							1250	3330			
12FHH	8	11.75	13.00	7							2450	4500			
	10	13.88	13.00	7							2175	4250			
	12	16.38	13.00	7							1250	3330			
12DEH	10	13.88	11.75	8							2175	4250			
13CL	8	11.75	12.50	6							2600				
	10	13.88	12.50	6							2175				
13CM	8	11.75	12.50	6							2600				
	10	13.88	12.50	6							2175				
13EH	8	11.75	13.00	6							2450	2990			
	10	13.88	13.00	6							2175	4250			
14RL	12	16.38	17.00	8.5							990	3075			
14RM	12	16.38	17.00	8.5							990	3075			
14RH	12	16.38	17.00	8.5							990	3075			
14EM	10	13.88	14.75	9								3950			
14FHM	12	16.38	17.00	8.5								3075	6930		
14FHH	12	16.38	17.00	8.5								3075	6930		
15EH	10	13.88	15.00	9								3860	7700		
	12	16.38	15.00	9								3330	7180		
16GM	12	16.38	17.25	8.5								2970	6800		
	14	17.63	17.25	8.5								2810	6650		
17EH	12	16.38	16.92	10								3110			
	14	17.63	16.92	10								2810	6960	11650	
17EM	12	16.38	18.00	10								2650	6502		
	14	17.63	18.00	10								2650	6502		
18GL	12	16.38	17.25	8.12								2970	6825		
	14	17.63	17.25	8.12								2810	6825		
18GM	12	16.38	17.25	8.12								2970	6825		
	14	17.63	17.25	8.12								2810	6664		
19GM	14	17.63	17.25	8.75								2810	6664	11390	
	16	20.00	17.25	8.75								1710	2990	10307	
19GH	14	17.63	17.25	8.75								2810	6664	11390	
	16	20.00	17.25	8.75								1710	2990	10307	
20TML	14	17.63	21.50	11									5190	9930	15500
	16	20.00	21.50	11									5190	9930	15500

SUCTION CAN SELECTION CHART

Layne/Verti-Line Model	Column Size	Flange O.D.	Max. Bowl O.D.	Clearance (A)	Allowable Capacity (GPM) at a Velocity of 5 Ft./Sec.									
					Can O.D. (D1)									
					30	36	42	48	54	60	72	84	96	
21EH	14	17.63	20.75	10	5190	9930	15500							
	16	20.00	20.75	10	5190	9930	15500							
22GM	14	17.63	22.50	11.25	4270	9000								
	16	20.00	22.50	11.25	4270	9000								
22GH	14	17.63	22.50	11.25	4270	9000								
	16	20.00	22.50	11.25	4270	9000								
23EHL	16	20.00	29.00	14		4918	10523	17016						
	18	22.00	29.00	14		4918	10523	17016						
	20	24.50	29.00	14		4918	10523	17016						
23EHM	16	20.00	29.00	14		4918	10523	17016						
	18	22.00	29.00	14		4918	10523	17016						
	20	24.50	29.00	14		4918	10523	17016						
23EHH	16	20.00	29.00	14		4918	10523	17016						
	18	22.00	29.00	14		4918	10523	17016						
	20	24.50	29.00	14		4918	10523	17016						
24GM	16	20.00	24.00	11.25	3418	8150	13923							
	18	22.00	24.00	11.25	3418	8150	13923							
27EM	18	22.00	28.11	14		5532	11145	17638						
	20	24.25	28.11	14		5532	11145	17638						
27EML	18	22.00	28.11	14		5532	11145	17638						
	20	24.25	28.11	14		5532	11145	17638						
30GM	20	24.25	27.75	13.50		5775	11390	17884						
	24	28.50	27.75	13.50		5262	10875	17368						
30GH	20	24.25	27.75	13.50		5775	11390	17884						
	24	28.50	27.75	13.50		5262	10875	17368						
31EM	20	24.25	31.30	15			8829	15499	22957					
	24	28.50	31.30	15			8629	15499	22957					
33EHH	24	28.50	41.50	21				6240	13771	21868				
	30	34.50	41.50	21				6240	13771	21868				
34EH	24	28.50	34.75	18			6110	12679	20138					
	30	34.50	34.75	18			6110	12679	20138					
36GM	24	28.50	40	20				7824	15283	23633	43005			
	30	34.50	40	20				7824	15283	23633	43005			
36GH	24	28.50	40	20				7824	15283	23633	43005			
	30	34.50	40	20				7824	15283	23633	43005			
38HH	20	24.25	34.25	17.13			6537	13108	20584					
	24	28.50	34.25	17.13			6537	13108	20584					
38HOH	20	24.25	34.25	17.13			6537	13108	20584					
	24	28.50	34.25	17.13			6537	13108	20584					
42RKHC	24	28.50	43	20				4690	12064	20318	39468			
	30	34.50	43	20				4690	12064	20318	39468			
44GM	30	34.50	43	21.5				4690	12064	20318	39468			
	36	40.50	43	21.5				4690	12064	20318	39468			
44GH	30	34.50	43	21.5				4690	12064	20318	39468			
	36	40.50	43	21.5				4690	12064	20318	39468			
57EH	30	34.50	55	27							25087	47759	73953	
	36	40.50	55	27							25087	47759	73953	

SUCTION INLET SIZE LIMITATION

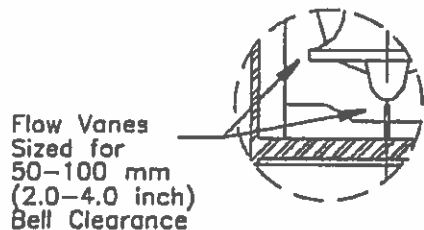
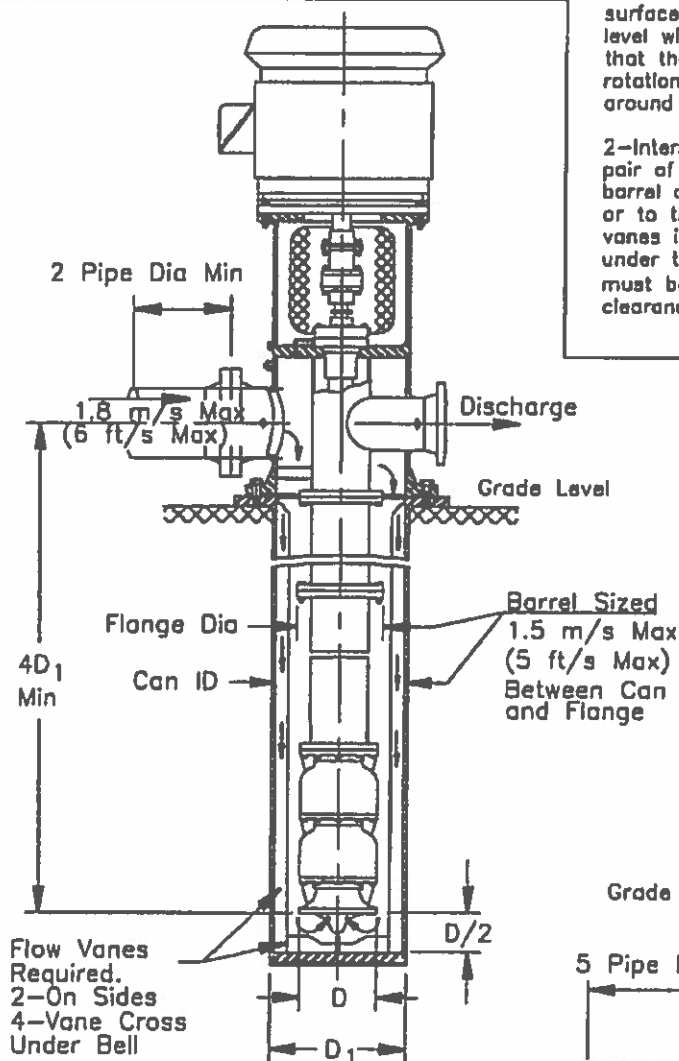
SIZE	MAXIMUM FLOW (GPM)	
	"L" AND CAST IRON HEADS	"T" HEADS
4"	159	238
6"	361	540
8"	625	935
10"	986	1474
12"	1414	2114
14"	1724	2577
16"	2283	3414
18"	2921	4368
20"	3638	5440
24"	5307	7936
30"	8399	12560
36"	12723	19026
42"	16705	24980
48"	21918	34177
54"	27838	41627
60"	34350	51525
72"	49675	74510

SUCTION CAN DESIGN STANDARD

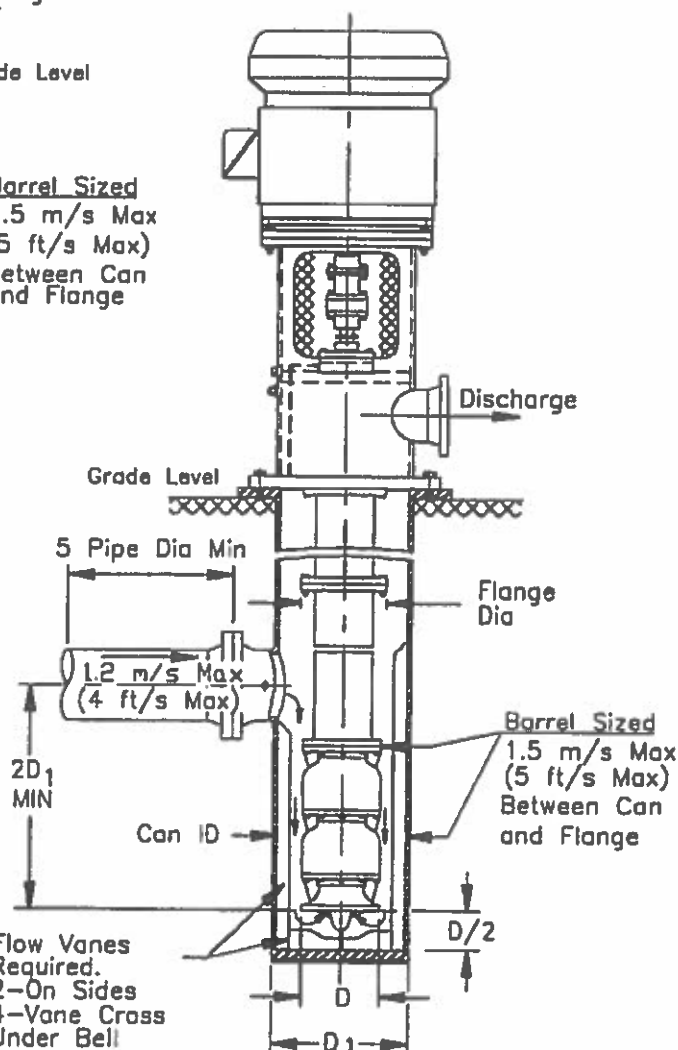
NOTE:

1—Care must be taken during installation of the can to assure concentricity of pump to can and that an out of level condition does not exist for the pump mounting surface. When cans are cast in concrete, the buoyancy forces placed on the can must be restrained to avoid having the can "move" out of level. Before installing the pump, the pump mounting surface must be checked to verify that the surface is level within 3 mm/mm (0.003 in/in) in all directions and that the pump will be centered in the can (to avoid rotational flow being generated by non-uniform flow around a non-concentric pump).

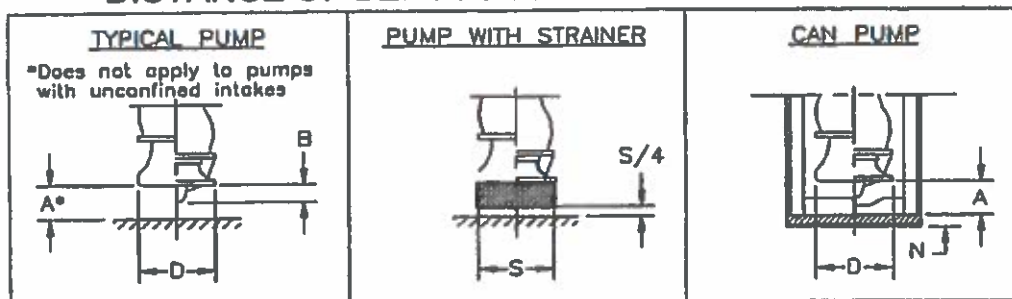
2—Internal flow straightening vanes are required. A pair of vanes should be centered on the inlet to the barrel and extended to above the normal liquid level or to the top of the barrel, as applicable. A set of vanes in the form of a cross should be provided under the pump bell. These flow straightening vanes must be designed to provide for 50–100mm (2.0–4.0 in) clearance to the suction bell.



D = Pump Suction Bell Dia
D₁ = Can Outside Dia



DISTANCE OF BELL TO FLOOR FOR TURBINE PUMPS



PUMP	A	B	D	S	PUMP	A	B	D	S
6DREL, 6DRMC	4	3.25	5.50	6.00	14RL, 14RH, 14RM	8.5	8.00	17.00	18.00
6EM	3	N/A	5.50	N/A	15EH	9	7.19	14.75	14.75
6RKLC, 6RKHC	4	3.25	5.50	6.00	16GM	8.5	3.00	17.25	18.00
6GM, 6GH	4	3.25	5.50	6.00	17EM	10	7.37	18.00	18.00
7EM	3	N/A	5.75	N/A	17EH	10	7.94	18.75	18.75
7CL, 7CEH, 7CM	3.75	0.75	7.50	8.00	18GL, 18GM	8.12	4.00	17.25	18.00
8EM	6	3.82	8.00	8.00	19GM, 19GH	8.75	2.75	17.25 ¹	18.00 ²
8RL, 8RM, 8RH	5	4.25	9.50	10.00	20TML	11	1.20	21.50	RTF
8URHC	4.5	3.88	7.50	8.00	21EH	10	5.19	20.75	20.75
8TM, 8TH	4.5	3.88	7.50	8.00	22GM, 22GH	11.25	6.25	22.5	23.00
10FHM, 10FHH	7	6.00	11.50	12.00	23EHH	14	2.50	29.00	29.00
10EM	7	4.93	10.00	10.00	23EHM	14	2.50	29.00	29.00
10RKLC, 10RKHC, 10RKEH, 10RKHS	5.5	4.00	9.50	10.00	23EHL	14	2.50	29.00	29.00
10TLC, 10THC	5	4.18	9.50	10.00	24GM	11.25	6.25	22.5	23.00
11EM	7	5.45	11.38	11.50	27EM, 27EMC	14	5.99	28.11	28.00
11EH	7	5.34	11.38	11.50	30GM, 30GH	13.5	4.75	27.00	27.50
12DEH	6	3.25	11.50	12.00	31EM	15	12.19	31.30	31.00
12FHL, 12FHM, 12FHH	7	6.50	13.00	13.62	33EHH	21	3.25	41.50	RTF
12EM	8	6.13	13.00	13.00	33HM	21	3.25	41.50	RTF
12RL, 12RM, 12RH	6.5	6.00	13.00	14.00	33HL	21	3.25	41.50	RTF
12RKBL, 12RKBM, 12RKBEH, 12RKBEH	6.25	5.30	11.50	12.00	34EH	16	N/A	32.00	31.00
12TLC, 12THC	5.75	4.80	11.50	12.00	38GM, 38GH	20	6.25	40.00	40.50
13CL, 13CM	6	3.00	11.50	12.00	38HH, 38HOH	17.13	3.00	34.25	34.75
13EH	6	4.13	13.00	13.00	42RKHC	20	6.00	40.00	40.50
14FHM, 14FHH	8.5	6.75	17.00	18.00	44GM, 44GHC	21.5	4.00	43.00	RTF
14EM	9	6.85	14.75	14.75	57EH	27	N/A	54.00	54.00

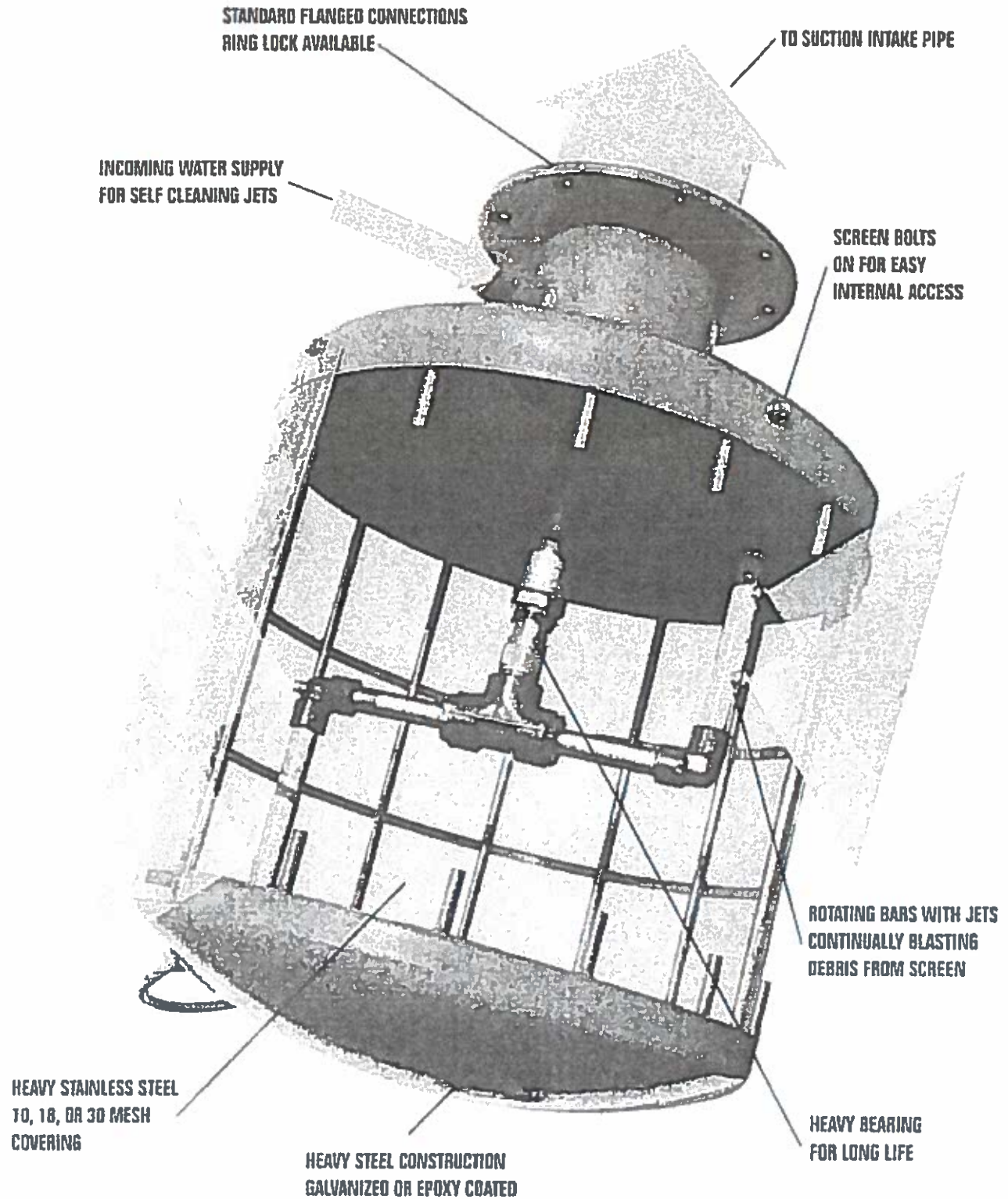
¹ Bell Diameter for wells or barrels. Bell diameter for sumps is 22.5".

² Basket diameter for wells or barrels. Basket diameter for sumps is 23".

Suction Pot	
Size	N
12	1.25
14	1.25
16	1.50
18	1.50
20	1.75
24	2.50
30	3.00
36	3.75
42	4.25
48	RTF
54	RTF
60	RTF
72	RTF
84	RTF
96	RTF

INTAKE SCREEN SPECIFICATIONS

Clearwater Self-Cleaning Suction Screen



If you irrigate, you know how important it is to keep equipment running smoothly and water flowing freely. Whether you are pumping water from a waste treatment facility, manure lagoon, stream, canal, river, irrigation ditch, pit or sump, or a golf course pond, you need the water to be free of trash and debris that could block water flow and damage the pump or clog water-distribution equipment.

The Clearwater Self-Cleaning Suction Screen is galvanized or epoxy coated and utilizes a heavy 10, 18, or 30 mesh stainless steel screen designed to increase pump efficiency. The screen continuously removes trash and debris from irrigation water that costs time and money in fuel, pumping efficiency and maintenance costs. And it can be used for agricultural, turf, industrial, centrifugal or turbine pump applications.

The suction screen is attached to the end of the pump in the water source. All water pulled in must

go through the screen before entering the intake pipe. The screen stops trash and debris from entering, plugging lines and causing costly maintenance repairs. The pump discharge return line drives two spray bars that continually rotate jet water at the screen and blast debris away from the screen at 35 to 100 PSI Operating Range.

The Clearwater screen — has no exterior moving parts that can break down or need repair. It can be installed at any altitude without the operation being affected and is uncollapsible and corrosion resistant. It also has a standard flanged connection, and other connections are available upon request. The Y Strainer or Mini Filter — an essential extra — provides easy access for cleaning and prevents the supply line to the screen and the spray nozzle from plugging.

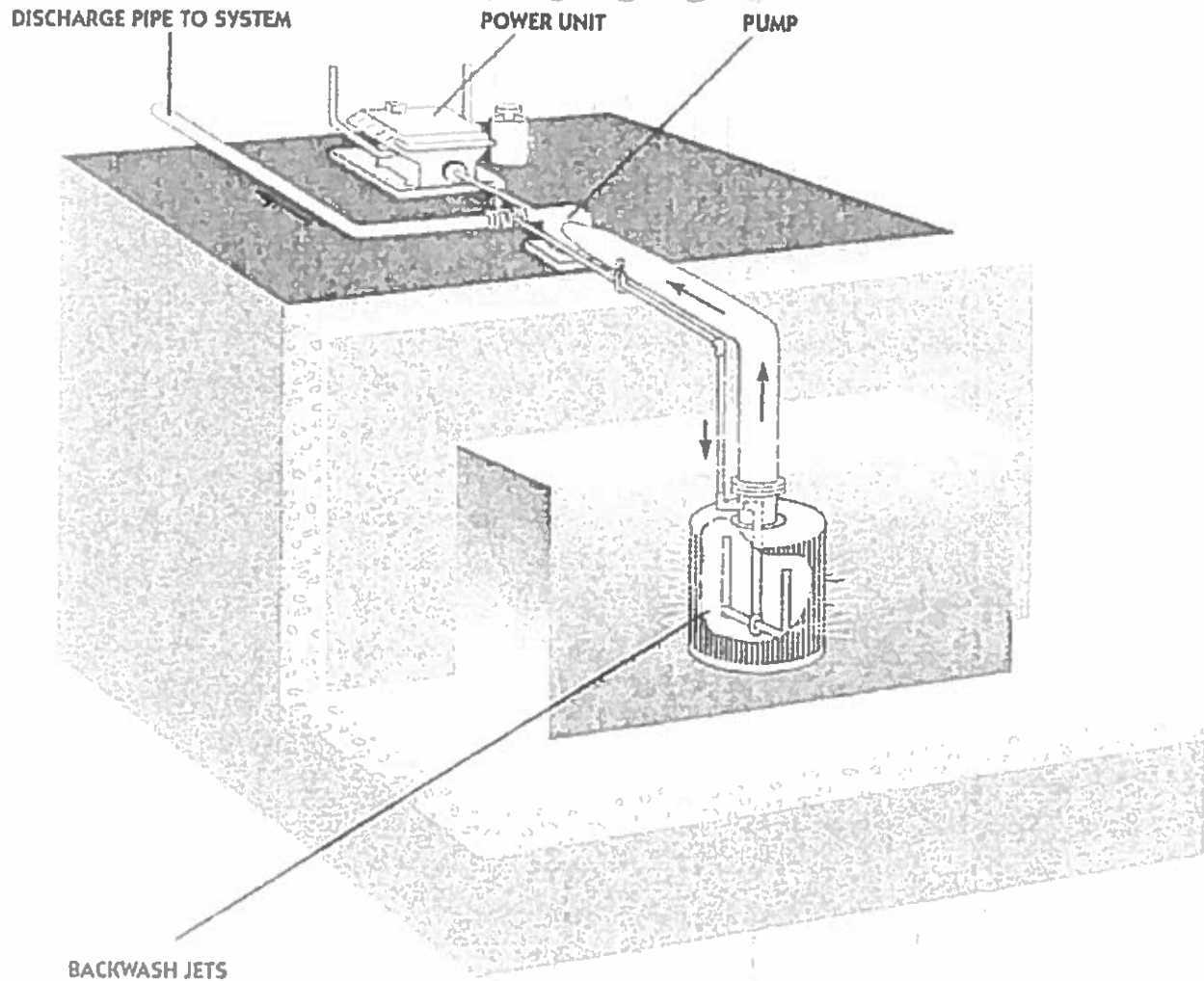
Let Clearwater clear your water for worry free irrigating!



Model	Flow U.S. GPM 10.18m	30M	Screen Length	Total Length	Diameter	Flange Size	Return Inlet	Minimum Operate. Pressure	Weight Lbs.	GPM Used To Operate
CW200	325	225	11"	25"	16"	4"	1 1/2"	35	58	20
CW400	550	400	15"	28 8"	16"	6"	1 1/2"	40	62	20
CW500	750	525	16"	32 5"	24"	8"	1 1/2"	40	102	20
CW800	950	700	18"	34 5"	24"	10"	1 1/2"	45	115	20
CW1000	1350	950	23"	39 5"	24"	10"	1 1/2"	50	123	28
CW1400	1650	1200	26"	42 5"	24"	12"	1 1/2"	55	131	28
CW1700	1950	1400	28"	44 5"	26"	12"	1 1/2"	55	148	28
CW2000	2350	1650	32"	48 5"	26"	14"	1 1/2"	60	160	36
CW2400	2600	1800	35"	52 5"	30"	16"	1 1/2"	65	223	36

SPECIFICATIONS

Typical Application



METRIC SPECIFICATIONS

Model	Flow M ³ /Hour		Screen Length MM	Total Length MM	Diameter MM	Flange Size MM	Return Inlet MM	Min. Operate Pressure Bars	Weight KG	Flow M ³ /Hour Used to Oper
	10 LPM	30M								
CW200	74	51	279	615	406	102	38	2.4	27	4.5
CW300	125	91	381	732	406	152	38	2.7	29	1.5
CW600	170	120	406	826	609	203	38	2.7	47	1.5
CW800	216	160	457	878	609	254	38	3.1	51	1.5
CW1000	307	216	504	1003	609	254	38	3.1	56	6.4
CW1400	375	273	660	1080	609	305	38	3.8	60	6.4
CW1700	441	319	711	1130	660	305	38	3.8	69	6.4
CW2000	534	375	819	1232	660	356	38	4.1	73	12.2
CW2100	591	409	889	1334	762	406	38	4.5	102	2.2

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CLEARWATER SELF-CLEANING SUCTION SCREEN

Price Information

Effective January 1, 2012

Clearwater Self-Cleaning Suction Screen

Clearwater Screens Operate In Any Position

MODEL	FLOW U.S. GPM		FISH SCREEN MAX. GPM FOR .4 FT. PER SEC.	SCREEN LENGTH	TOTAL LENGTH	DIAMETER	FLANGE SIZE	RETURN INLET	GALLONS USED TO OPERATE	STD. BRASS BEARING REC. OPERATING PRESSURE	SEALED BEARING REC. OPERATING PRESSURE	WEIGHT LBS.	OPTION VORTEX LIST PRICE	LIST PRICE
	12/18M	24M	12 MESH											
CW100	200	165	180	9"	19.5"	12"	3"	1/2"	12	40-60	N/A	30	\$ N/A	\$ 678.83
CW200	325	225	355	11"	25"	16"	4"	1 1/2"	20	40-60	40-100	58	104.60	960.57
CW400	550	400	485	15"	28.8"	16"	6"	1 1/2"	20	40-60	40-100	62	134.49	1208.63
CW600	750	525	775	16"	32.5"	24"	8"	1 1/2"	20	40-60	40-100	102	165.31	1432.41
CW800	950	700	875	18"	34.5"	24"	10"	1 1/2"	20	40-60	40-100	115	188.53	1482.29
CW1000	1350	950	1115	23"	39.5"	24"	10"	1 1/2"	28	40-60	40-100	123	215.49	1615.63
CW1400	1550	1075	1265	26"	42.5"	24"	12"	1 1/2"	28	40-60	40-100	131	267.00	1748.36
CW1700	1800	1250	1475	28"	44.5"	26"	12"	1 1/2"	28	40-60	40-100	148	283.07	1932.43
CW2000	2100	1450	1685	32"	48.5"	26"	14"	1 1/2"	36	40-60	40-100	180	331.94	2081.72
CW2400	2600	1800	2125	35"	52.5"	30"	16"	1 1/2"	36	40-65	40-100	223	412.91	2257.09
CW3000	3000	2075	2430	40"	57.5"	30"	16"	1 1/2"	44	40-65	40-100	236	449.74	2784.34
CW3500	3500	2420	2750	40"	59.5"	36"	18"	1 1/2"	44	40-65	40-100	283	491.90	3536.28
CW4000	4000	2765	3150	40"	63.5"	42"	18"	1 1/2"	44	40-65	40-100	258	491.90	4417.53
Mini Inline Filter – Model M150														449.83
Strainer (Clear) 1 1/2" Solvent Weld 60 to 70 GPM														101.39
Strainer (Clear) 2" Solvent Weld 70 to 100 GPM														143.01

Mini Inline Filter – Model M150

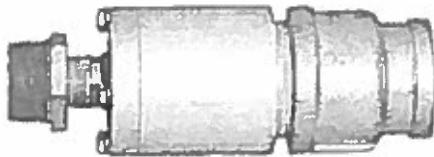
Strainer (Clear) 1 1/2" Solvent Weld 60 to 70 GPM } Purging Without Removing Screen
Strainer (Clear) 2" Solvent Weld 70 to 100 GPM

New Flow Entry Control Vortex Tube Option

Brass and Sealed Bearings Come In One Size – Fits All Models

NEW HIGH PRESSURE SEALED BEARING 40 - 100 P.S.I.

*Models 3000, 3500, and 4000
Offered Only with Sealed Bearing



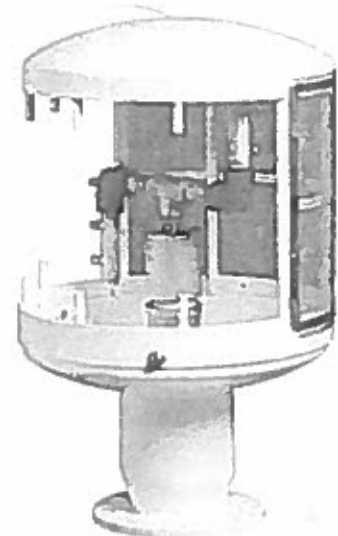
Mesh Sizes Available
4, 8, 12, 18, and 24

SEALED BEARING

Trouble free operation under the worst conditions.

40 P.S.I. required to operate sealed bearing. Add \$239.02 list to each C.W. for sealed bearing.

100 P.S.I. maximum operating pressure.



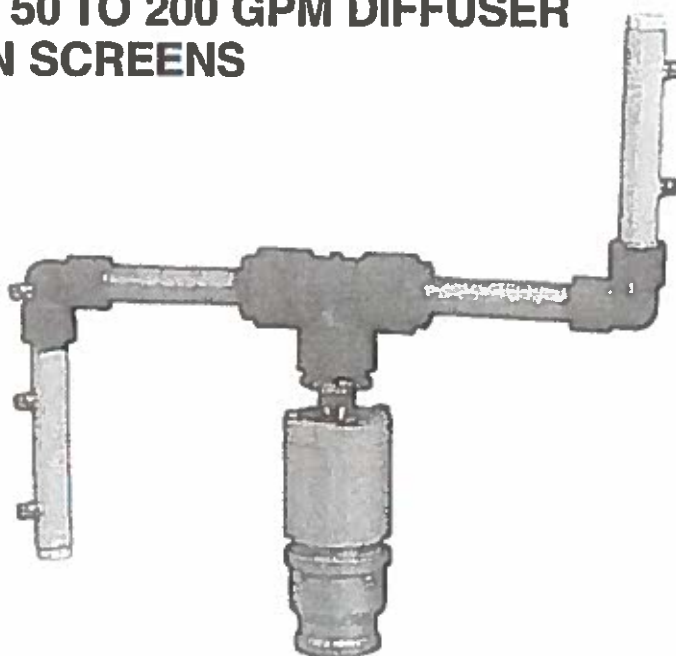
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CLEMONS
SALES CORPORATION

CLEARWATER PARTS – 50 TO 200 GPM DIFFUSER SUCTION SCREENS

Parts – Accessories

Replacement Bearing Brass	LIST PRICE \$228.29
Replacement Vee Jets	8.27
Replacement Vee Jets S.S.	20.01
Sealed Heavy Duty Bearing	439.85
Sealed Bearing Repair Kit	139.33
Sled Plates CW200 - 400	140.76
Sled Plates CW600 - 1700	279.48
Sled Plates CW2000 - 3000	372.30



MODEL	REPLACEMENT SPRAY ASSEMBLY LESS BEARING	REPLACEMENT 12 MESH SCREEN	REPLACEMENT 18 & 24 MESH SCREEN
	LIST PRICE	LIST PRICE	LIST PRICE
CW200	\$158.08	\$ 56.88	\$ 80.01
CW400	161.68	72.05	101.30
CW600	165.53	117.21	164.77
CW800	169.26	130.41	183.35
CW1000	182.57	163.68	228.48
CW1400	186.60	182.02	255.88
CW1700	190.45	211.07	296.73
CW2000	203.81	238.97	335.90
CW2400	207.50	299.14	420.53
CW3000	212.70	351.73	493.66
CW3500	253.52	421.84	590.59
CW4000	294.34	492.01	688.82

50 To 200 GPM Diffuser Style Suction Screen

MODEL	MAX. GPM RATING	INLET CONNECTION	OVERALL LENGTH	DIAMETER	STANDARD S.S. SCREEN	WEIGHT	LIST PRICE
DS50	0-50	2" FPT	15 3/4"	6"	3/32" Perf.	11	\$259.65
DS100	50-100	3" FPT	18 1/4"	8"	3/32" Perf.	15	329.82
DS200	100-200	4" FPT	25"	10"	3/32" Perf.	24	406.80



No. DS400

2" Threaded Brass Check Valve	LIST PRICE \$ 58.12
3" Threaded Brass Check Valve	168.16
4" Threaded Brass Check Valve	268.89



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Installation and Operating Instructions for Clearwater Self-Cleaning Suction Screen

1. Before installing a CW Screen, check pumping system's pressure. If pumping with very low pressure, a booster pump may be required. Booster pump not supplied by Clemons. Consult specifications in CW brochure for recommended operation pressure. Higher pressure may be required for certain applications. Consult our factory.
2. Do not install a backwash line smaller than 1 ½". If your CW Screen will be located more than 100 feet from the pump a somewhat larger line may be necessary to overcome friction loss.
3. Check your CW specifications to be sure you don't exceed CW's maximum flow range. It may be less with some applications with excessive debris. For fisheries consult our factory.
4. Thoroughly flush the backwash line before attaching it to you CW screen. Failure to do this could result in plugging spray jets inside the screen.
5. Your CW Screen should not be located any closer than 6 inches to any object.
6. Install your CW Screen's flanged outlet to pump's suction/inlet pipe. If other adapter is desired instead of flange, please contact the factory. Plumb the backwash line into your pump's discharge pipe. It is not recommended to use the threaded plug holes in the pump case because there may not be enough pressure or water volume to operate the screen.
7. Backwash line should be plumbed ahead of the main line's butterfly valve. The butterfly can be partially closed to create sufficient back pressure during start-up.
8. These items are to be installed on the backwash line (starting from the pump discharge to the CW screen) in the following order: One properly sized gate or ball valve (at least 1-1/2" or larger), One inline 18 mesh strainer (at least 1-1/2" or larger) and one pressure gauge (liquid filled recommended).
9. If necessary, access to the internal parts of your CW Screen is very simple. Three bolts remove the entire screened area for complete access to all internal parts. Special access plate upon request.
10. Your CW Screen does not need more than 7 inches of submergence because the self-cleaning action breaks up any vortex that might form.

Over

11. Your CW Screen with internal rotation spray bars lets you avoid complicated set-ups. Your CW Screen is rugged steel galvanized or epoxy coated body with heavy gauge stainless steel mesh screen. The CW Screen is versatile and affordable for self cleaning pump suction applications.

12. Some extreme applications conditions could be too harsh for the Clearwater screens to work properly. In extreme moss or dairy applications consult the factory.

SPECIFICATIONS

Model	Flow U.S. GPM 12/18m	30M	Screen Length	Total Length	Diameter	Flange Size	Return Inlet	Operate. Pressure	Weight Lbs.	GPM Used To Operate	Fish Screen Max GP For 4ft Per Sec
CW200	325	225	11"	25"	16"	4"	1 ½"	40-60	58	20	355
CW400	550	400	15"	28.8"	16"	6"	1 ½"	40-60	62	20	485
CW600	750	525	16"	32.5"	24"	8"	1 ½"	40-60	102	20	775
CW800	950	700	18"	34.5"	24"	10"	1 ½"	40-60	115	20	875
CW1000	1350	950	23"	39.5"	24"	10"	1 ½"	40-60	123	28	1115
CW1400	1550	1075	26"	42.5"	24"	12"	1 ½"	40-60	131	28	1265
CW1700	1800	1250	28"	44.5"	26"	12"	1 ½"	40-60	148	28	1475
CW2000	2100	1450	32"	48.5"	26"	14"	1 ½"	40-60	160	36	1685
CW2400	2600	1800	35"	52.5"	30"	16"	1 ½"	40-65	223	36	2125
CW3000	3000	2075	40"	57.5"	30"	16"	1 ½"	40-65	236	44	2430
CW3500	3500	2420	40"	59.5"	36"	18"	1 ½"	40-65	283	44	2750
CW4000	4000	2765	40"	63.5"	42"	18"	1 ½"	40-65	358	44	3150

METRIC SPECIFICATIONS

Model	Flow M3/Hour 12/18m	30M	Screen Length MM	Total Length MM	Diameter MM	Flange Size MM	Return Inlet MM	Min. Operate Pressure Bars	Weight KG	Flow M3/Hour Used To Oper.
CW200	74	51	279	635	406	102	38	2.4	27	4.5
CW400	125	91	381	732	406	152	38	2.7	29	4.5
CW600	170	120	406	826	609	203	38	2.7	47	4.5
CW800	216	160	457	876	609	254	38	3.1	53	4.5
CW1000	307	216	584	1003	609	254	38	3.4	56	6.4
CW1400	352	247	660	1080	609	305	38	3.8	60	6.4
CW1700	409	288	711	1130	660	305	38	3.8	68	6.4
CW2000	477	336	813	1232	660	356	38	4.1	73	8.2
CW2400	591	409	889	1134	762	406	38	4.5	102	8.2
CW3000	682	480	1016	1461	762	406	38	4.5	105	10.0
CW3500	795	550	1016	1511	915	457	38	4.5	127	10.0
CW4000	909	628	1016	1613	1067	457	38	4.5	160	10.0

MAXIMUM ICE DEPTH CALCULATIONS

Calculation of Ice Thickness for

Herron Creek Fire H₂O Pond

This projection has been calculated based upon 2013 Helena Montana weather data provided by Weather Underground ¹, a website that specializes in current, future, and past weather conditions.

Method:

Stefan's Equation

$$t_i = C(AFDD)^{.5}$$

where t_i is the expected thickness of ice, C is the coefficient of growth, and AFDD is the accumulated freezing degree days from FDD(0) to FDD(e). FDD(0) is 11/16/2013 and FDD(e) is 3/2/2014. A freezing degree day is defined to be $FDD=(32-T_a)$, where T_a is the average temperature within a 24 hour period. The AFDD for Helena is calculated at 887 from FDD(0) to FDD(e). The expected ice thickness is shown on the table below with various values of C.

C	Ti (ICE THICKNESS IN INCHES)	
0.12	3.573905427	
0.15	4.467381784	
0.21	6.254334497	
0.41	12.21084354	
0.5	14.89127261	
0.6	17.86952713	Recommended Design Thickness
0.7	20.84778166	
0.8	23.82603618	

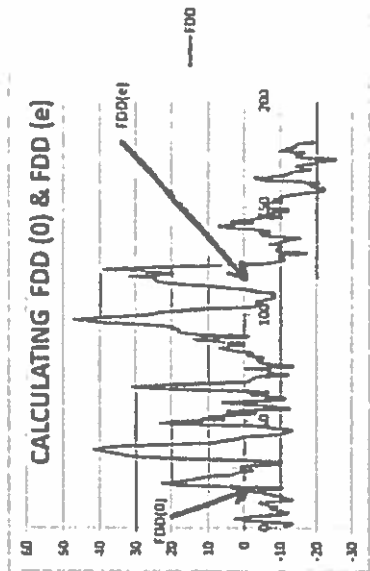
It should be noted that snow overtop of the ice will form an insulation which will cause the value of C to lower. Conversely, if ice cover growth is affected by underturning, shoving, or frazil deposition, the value of C will increase ². The range of "C" for an average lake with snow is 0.5-0.7. We recommend a design ice thickness of 17.87" at C=0.60.

1. <http://www.wunderground.com/history/airport/KHLN/2014/4/2/MonthlyHistory.html?>

2. *Ice Engineering*, 2004. Us Army Corps of Engineers, Cold Regions Research & Engineering Laboratory.

NET FDD	FDD(0)	FDD(e)	C	T _i (ICE THICKNESS IN INCHES)
887	11/16/2013	3/2/2014	0.12	3.573905427
887			0.15	4.467341784
887			0.21	6.254334497
887			0.31	12.31084354
887			0.5	14.89127261
887			0.6	17.36951713
887			0.7	20.84778166
887			0.8	23.82603618

Conclusions Used



Max Temperature	Mean Temperature	Min Temperature	FDD (FREEZING DEGREE DAY)
55	43	30	-11
60	45	30	-13
42	35	28	-3
37	29	20	3
42	33	23	-4
47	39	31	-7
53	44	34	-12
40	41	36	-9
46	39	31	-7
50	41	31	-9
47	36	29	-4
51	36	21	-4
50	45	34	-13
50	43	36	-11
45	41	37	-9
44	34	32	-6
41	34	26	-2
51	38	25	-6
54	42	25	-10
25	13	1	19
22	9	-4	23
29	15	1	17
31	18	4	14
33	21	9	11
41	28	15	-4
41	30	18	2
44	34	24	-2
40	29	17	3
45	31	17	1
47	41	35	-9
48	42	36	-10
42	27	11	5
11	7	2	75
7	0	-7	32
6	-1	-12	35
3	7	-11	39
-4	10	-17	42
3	-6	-15	38
25	7	-11	25
28	23	18	9
35	26	17	6
38	30	21	2
43	32	21	0
47	41	34	-9
54	43	32	-11
51	45	38	13
52	40	37	-8
51	33	14	-1
14	9	4	23
20	12	-4	20
33	26	19	6
32	20	7	12
39	26	13	6
39	35	30	-3
39	27	14	5
50	44	38	-12
50	40	30	-8

12/24/2013	-49	33	16	-1
12/25/2013	38	26	13	6
12/30/2013	-45	38	30	-6
12/31/2013	-47	-43	38	.11
1/1/2014	-42	36	29	-4
1/2/2014	-42	33	23	-1
1/3/2014	53	38	23	-6
1/4/2014	25	16	6	16
1/5/2014	7	1	-6	31
1/6/2014	17	7	-4	25
1/7/2014	28	22	16	10
1/8/2014	-41	33	25	-1
1/9/2014	-42	34	26	-2
1/10/2014	-45	35	25	-3
1/11/2014	55	-44	32	-11
1/12/2014	-41	36	30	-4
1/13/2014	-48	39	29	-7
1/14/2014	-47	32	17	0
1/15/2014	50	-45	39	-13
1/16/2014	50	39	28	-7
1/17/2014	52	36	20	-4
1/18/2014	-49	35	24	-3
1/19/2014	54	37	20	-5
1/20/2014	-45	33	20	-1
1/21/2014	-47	34	20	-2
1/22/2014	34	40	26	2
1/23/2014	33	25	16	7
1/24/2014	39	25	10	7
1/25/2014	-40	31	15	1
1/26/2014	-41	11	20	1
1/27/2014	28	19	9	13
1/28/2014	35	18	1	14
1/29/2014	-41	33	25	-1
1/30/2014	25	18	30	14
1/31/2014	22	14	6	18
2/1/2014	23	13	4	18
2/2/2014	19	12	4	20
2/3/2014	17	9	1	23
2/4/2014	2	-4	-11	36
2/5/2014	-2	-11	-21	-43
2/6/2014	5	-15	-26	-47
2/7/2014	6	-6	-18	38
2/8/2014	13	5	-3	27
2/9/2014	13	8	2	24
2/10/2014	-21	14	6	18
2/11/2014	-40	22	4	10
2/12/2014	50	35	19	-3
2/13/2014	-45	37	28	-5
2/14/2014	-43	35	28	-3
2/15/2014	-46	37	28	-5
2/16/2014	-47	40	32	-8
2/17/2014	51	-40	28	-8
2/18/2014	-48	-40	32	8
2/19/2014	-44	35	26	-3
2/20/2014	39	32	24	0
2/21/2014	34	26	18	6
2/22/2014	23	19	12	14
2/23/2014	15	10	4	22

2/24/2014	11	7	3	25
2/25/2014	19	7	5	25
2/26/2014	12	0	-12	32
2/27/2014	25	12	-1	20
2/28/2014	20	9	-3	23
3/1/2014	-3	-7	-12	39
3/2/2014	6	3	-12	35
3/3/2014	42	22	2	10
3/4/2014	48	17	26	5
3/5/2014	52	41	30	-9
3/6/2014	50	43	36	-11
3/7/2014	48	42	35	-10
3/8/2014	51	41	30	-9
3/9/2014	62	43	36	-17
3/10/2014	45	39	33	-7
3/11/2014	48	40	31	-8
3/12/2014	53	42	31	-10
3/13/2014	53	38	23	-6
3/14/2014	53	42	31	-10
3/15/2014	50	44	37	-12
3/16/2014	65	47	29	-15
3/17/2014	44	33	31	-6
3/18/2014	42	36	30	-4
3/19/2014	50	39	27	-7
3/20/2014	41	34	27	-2
3/21/2014	12	25	18	7
3/22/2014	36	25	13	7
3/23/2014	46	34	22	-2
3/24/2014	34	28	22	3
3/25/2014	50	35	19	-3
3/26/2014	53	42	30	-10
3/27/2014	41	34	26	-2
3/28/2014	50	39	22	-7
3/29/2014	51	44	36	-12
3/30/2014	48	35	30	-7
3/31/2014	47	38	28	-6
4/1/2014	47	37	26	-5
4/2/2014	52	42	32	-10
4/3/2014	55	40	25	-8
4/4/2014	56	42	27	-10
4/5/2014	52	44	35	-12
4/6/2014	50	48	39	-16
4/7/2014	63	53	42	-21
4/8/2014	73	54	35	-22
4/9/2014	61	50	38	18
4/10/2014	60	49	38	-17
4/11/2014	66	52	38	-20
4/12/2014	48	38	27	-6
4/13/2014	44	34	23	-2
4/14/2014	42	41	19	-9
4/15/2014	53	44	34	12
4/16/2014	54	45	36	-13
4/17/2014	63	50	37	-18
4/18/2014	54	47	39	-15
4/19/2014	67	46	34	-14
4/20/2014	62	51	40	-19
4/21/2014	71	52	32	-20
4/22/2014	73	57	41	-25

4/23/2014	52	-5	38	-13
4/24/2014	57	-6	35	-14
4/25/2014	60	-4	35	-16
4/26/2014	46	-1	35	-8
4/27/2014	57	-4	30	-12
4/28/2014	54	-6	37	-14
4/29/2014	60	-5	38	-14
4/30/2014	68	51	33	-19

FIRE FILL WELL

From: "Ryan Casne, PE" <ryan@casneinc.com> 17-Mar-2015 15:41
<ryan@casneinc.com>
To: bdreyer@dowl.com <bdreyer@dowl.com>
CC: Greg McNally <gmcnally@lccountymt.gov>, 'Ron Bartsch - Sussex'
<rbartsch@sussexconstruction.com>
Subject: Updated Herron Creek Fire System Detail Plan
Attachments: INTERNET (1763 bytes)
MESSAGE HTML (6707 bytes)
MESSAGE TEXT (1812 bytes)
Herron CreekFire Supression Sy (282208 bytes)
Mime.822 (408142 bytes)
image002.jpg (7116 bytes)

Hi Bill,

It was a pleasure talking to you this morning about the Herron Creek fire suppression system and your subsequent review. Iâ€™ve updated the attached drawing to reflect your suggestions. The changes are summarized as follows:

The dry hydrant has been changed to a standard Mueller Centurion or Super Centurion; painted yellow.

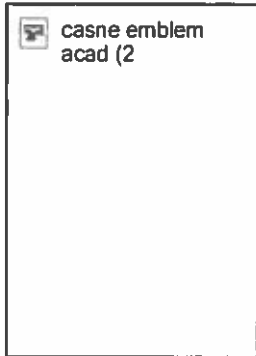
A ^{2 inch} ~~2 1/2~~ diameter SCH40 PVC circulation line has been shown at the hydrant and terminates within the pond near the dry hydrant strainer.

The self-cleaning intake strainer has been detailed to show a minimum ^{18 inch} ~~18 1/2~~ of separation between the pond bottom and the bottom on the strainer/intake. The purpose is to allow for silting of the pond.

You had suggested installing the intake strainer horizontally rather than vertically. I spoke with the strainer manufacturer (Clemmons) and although the strainer is rated for installation at any attitude they recommend it be installed vertically for the best self-cleaning performance.

Please let me know if you have any further questions. Thanks again Bill,

Ryan Casne, PE
Senior Engineer, Principal
CASNE & ASSOCIATES INC.
ryan@casneinc.com
(406) 443-1656



This communication (including attachments) contains private, confidential, privileged and/or proprietary information intended solely for the Recipient(s) named above. If you are not the intended Recipient, any use, dissemination, distribution or copying of the communication is strictly prohibited. If received in error, we apologize and ask that you please notify the Sender by calling (406) 443-1656 or via return e-mail, permanently delete this communication from your computer and destroy any printed copies. Thank you in advance for your cooperation.



March 27, 2015

Greg McNally, Planner II
Lewis and Clark County
Community Development and Planning
316 N. Park Avenue
Helena, MT 59601

Subject: Heron Creek Subdivision Review

I have conducted a review of the Heron Creek Subdivision's water supply proposal for compliance with the "effective and efficient" language. The documents used are:

- Heron Creek Fire Protection 3-6-15.pdf
- Herron Creek Fire Suppression System REV3-17-2015.pdf
- The National Fire Protection Association *Uniform Fire Code* and Standard 1142 – *Standard on Water Supplies for Suburban and Rural Fire Fighting*.

Heron Creek Fire Protection/Suppression System

The "central fire protection system with hydrants" agreement utilizes a fire pond as water storage, two pressurized hydrants, and one draft hydrant. It appears to include all items of design and maintenance that would be standard for this application, including performance testing criteria.

Recommendation: The connections from the draft hydrant and the recirculation line be standard fire service connections and are reviewed and approved by the Tri-Lakes Fire Department.

NFPA 1/Uniform Fire Code and NFPA 1142

At the time of application, the adopted Fire Code for Montana, NFPA 1/Uniform Fire Code (2003 ed.), requires a water supply in §18.3.1 and §18.3.2. Annex A provides further explanatory material specifically in §A.18.3.2 which states:

"The following documents can serve as a reference for additional water supply and fire flow information: NFPA 1141, *Standard for Fire Protection in Planned Building Groups* and NFPA 1142, *Standard on Water Supplies for Suburban and Rural Fire Fighting*. "

In my opinion, the above proposal meets the intent of the Fire Code in both delivery and duration of the water supply.

Conclusion

It is my opinion that the proposed "central fire protection system with hydrants", as submitted, does appear to be in compliance with the "effective and efficient" language.

Bryan Connelley,
Fire Out Consulting, PLLC
PO Box 407
Belgrade, MT 59714
(406) 570-0506
Bryan@Fireoutconsulting.com



March 24, 2015

Director of Community Development & Planning
Attn: George Theborge, AICP
316 North Park Ave.
Helena, MT 59623

RE: Heron Creek Subdivision Review

Dear George:

The plans and supplemental information relating to the Heron Creek Subdivision's Fire Water Pumping System have been reviewed as requested by Lewis Clark County and have been found to be appropriate and adequate to supply a sufficient and reliable fire protection water facility for the proposed subdivision.

DOWL's review consisted of:

1. Fire pond volume requirements.
2. Pond freezing thickness and sediment depth requirements.
3. Pump sizing requirements.
4. Draft Hydrant Requirements (Please note; suction head requirements for the fire department's trucks are not known. Flow rates for the draft hydrant may vary based on fire department pump sizes).

Please feel free to call at your convenience if you have any questions.

Sincerely,
DOWL

William Dreyer, P.E.
Senior Civil Engineer
bdreyer@dowl.com
Ph. 406-586-8834



Tri-Lakes Volunteer Fire Department

3200 Spokane Creek Road
East Helena, MT 59635

Phone & Fax: 406.475.3552

June 23, 2015

Greg McNally
Lewis & Clark County
Community Development and Planning
316 N. Park Ave.
Helena, MT 59623

Dear Greg:

The purpose of this letter is to provide comments related to the Heron Creek Subdivision as requested by your letter dated June 18, 2015.

I have reviewed the information about the fire suppression system dated March 6, 2015 from Casne & Associates, Inc. The information and specifications are consistent with the discussions that we had with Mr. Bartsch, Mr. Bartsch's attorney – Cherche Prezeau, and Mr. Casne on Monday, March 2nd.

The plans call for 1,000 gpm pressurized to a minimum of 20 psi from two fire hydrants that provide access points within 1,000 ft. of every house in the subdivision. The fire water is provided from two man-made lined ponds, the first of which is a settling pond to minimize sediment and debris from the main pond. The developer and the engineer have responded to our concerns about debris by proposing a self-cleaning strainer. A dry hydrant connection was also added for redundancy in case of electrical outage since there is no direct vehicle access to the pond. The current proposal has brought the open water storage concept's reliability as high as it reasonably can. In addition a funding mechanism has been outlined for the homeowners association to own and maintain the installation.

However, the one concern we have voiced consistently in the process for the last 8 years is the density of the center oval. The original design had 22 duplex condos in the oval which was then changed in 2011 to 43 single family lots with the smallest lot at 0.16 acres. The density simply cannot be protected given Tri-Lakes Volunteer Fire Department's capabilities and limitations of our all-volunteer force. The developer proposed on November 26, 2014 to install fire sprinklers in the inhabited structures on all lots less than one acre. We loved the idea but legal ruled that any sprinkler provisions would be unenforceable.

Our concern still exists in the current plan since it does not address our "gentlemen's agreement" that was made at the March meeting between Tri-Lakes Fire and Mr. Bartsch that Mr. Bartsch will install or make sure that all builders will install NFPA 13D fire sprinklers in all of the inhabited structures built on lots 66 through 109. There is no mention of it anywhere in the application. We believe written documentation and the covenants on lots 66 through 109 should reflect that the gentlemen's agreement has been made and its provisions. Legal took the position the County could not force the developer to put the sprinklers in and probably could not enforce

Page 2

the covenants if they were not complied with but that should not preclude the developer from stating his intention and putting the resulting covenants on lots 66 through 109 voluntarily.

As far as we are concerned the application is not complete without the provisions needed to document to all purchasers and builders the voluntary requirements placed on those lots by the developer.

Without those voluntary provisions, we are back to the same place we have been all along – We cannot protect the center of the subdivision given our current capabilities. The risk of fire spreading from house to house in the center oval is too great and we CANNOT say we can protect them when we believe we cannot.

We have been consistent in our alarm about protecting the center of this subdivision. I am enclosing the developer proposed sprinkler provisions from November 2014, our response to the request for comments in April 2014, and our response to comments in January 2012. The developer already provided the original agreement between us in 2007 although it is not very relevant given the substantial changes from the original subdivision since 2007.

Thank you for the opportunity to comment again. We would certainly like to get the subdivision done after 8 years of work but we will not shirk our responsibilities to those residents that will someday occupy those 43 houses or the our volunteer firefighters that must protect them.

Sincerely,
TRI-LAKE VOLUNTEER FIRE DEPARTMENT

A handwritten signature in blue ink, appearing to read "Robert J. Drake", with a stylized flourish at the end.

Robert J. Drake, Fire Chief


November 26, 2014

Chief Bob Drake
Tri-Lakes VFD
3020 Spokane Creek Rd
East Helena, MT 59635

**RE: Fire Suppression Improvements Agreement
Heron Creek Subdivision**

Dear Bob:

This letter has been written in follow-up to our meeting with Ron Bartsch on November 11th. Below is a list of the agreed upon fire protection improvements that will be implemented within the Herron Creek subdivision to comply with the Lewis & Clark County conditions of final plat approval which read: "The Applicant and the County must agree, prior to final plat approval, on fire protection measures that minimize the risk of fire and that permit the effective and efficient suppression of fires."

- 1) There will be a total of 109 Lots within Herron Creek Subdivision 66 Lots will contain gross acreage of less than 1.00 Acre.
 - 2) All inhabited structures on lots of less than 1.00 Acre shall be sprinkled in accordance with NFPA 13D (2013 edition).
 - 3) The structure sprinkling requirement shall be reflected in the Herron Creek restrictive covenants, filed with the Lewis & Clark County Clerk and Recorder. The covenants will be written so that the future HOA cannot vote the sprinkling requirement out.
 - 4) The existing home located on Lot 65-Phase I (0.92 Acres) shall be exempted from the sprinkling requirements.
 - 5) In addition to the NFPA 13D fire sprinkler requirements listed above, Herron Creek shall also contain a central fire protection system with hydrants.
 - 6) The system shall provide a flow of 500 GPM at a minimum of 20PSI, continuously for a minimum of two hours.
 - 7) The system shall contain two (2) hydrants. The hydrants shall be located within 1000' of each home within the Herron Creek Subdivision.
 - 8) Fire water storage will consist of an existing, lined, open-water pond. The pond will contain the required volume 365 days/year regardless of ice buildup.
- 

- 9) The pumping system will consist of a centrifugal pump, pressure transducer, and valving located within a heated below-grade pump vault. The pumping system will be functional 365 days/year.
- 10) A Clemons® Clearwater self-cleaning suction screen (10" diameter, Model CW1000) will be added to the existing intake strainer to mitigate pump intake clogging due to debris. The unit will be pressurized and fed water using the same fire pump that feeds the hydrants and therefore will operate simultaneously and automatically when a pump is activated.
- 11) The pond will continually be refilled as needed by a dedicated well. The well will fill the pond when commanded by a pressure transducer located within the pump vault. The refill system will function 365 days/year.
- 12) The fire water pump will be activated via switches located at each fire hydrant.
- 13) The fire water system shall be maintained without funding from an RID. Responsibility for maintenance and funding for such shall be by the Herron Creek HOA as required within the Declaration of Covenants.
- 14) The Declaration of Covenants shall require a joint account be created for the sole purpose of fire system maintenance. Five percent (5%) of the annual HOA dues will be diverted into this account until the balance reaches \$20,000.00. The fund will then be maintained at this amount until maintenance is needed. The five percent (5%) contribution shall resume each time the account balance falls below \$20,000.00. The covenants will be written so that the future HOA cannot vote the fire suppression funding mechanism out.
- 15) Easements will be recorded on the final plat to ensure the fire pumping system, pond, piping, and all related appurtenances can be maintained and/or replaced when needed.
- 16) Roadways and parking areas will be designed to help ensure emergency access to fire hydrants.
- 17) If bollards are installed within the emergency access route between Lots 55 & 56 and the access to the drainfield area located between Lots 1 & 2, they shall be removable.
- 18) As part of the maintenance of the community and in compliance with the Vegetation Management Plan, the parks and wastewater facility areas will be maintained as parkland. The grasses will be mowed and the trees maintained. All lots will be required to maintain mowed grass or landscaping on the entire lot.

lcl

This proposal and agreement represents the entire and integrated agreement between the parties and shall supersede all prior agreements and/or negotiations whether written or oral.

*Tri-Lakes Vol. Fire Dept by
Bob J. Drake, Chief*

Ron Bartsch, Owner

Bob Drake, Fire Chief

led



Tri-Lakes Volunteer Fire Department

3200 Spokane Creek Road
East Helena, MT 59635

Phone & Fax: 406.475.3552

April 22, 2014

*Actually
sent on 4/30/14*

Greg McNally
Lewis & Clark County
Community Development and Planning
316 N. Park Ave.
Helena, MT 59623

Dear Greg:

The purpose of this letter is to provide comments related to the Heron Creek Subdivision fire protection provisions.

We have been dealing with this concept and the first installed system for some time. We have tested the existing system twice with dismal results and realized early on that the developer was not taking the fire suppression system seriously. We are heartened to see the first proposed pump system has been completely replaced with a larger system but our ongoing concerns related to reliability and future maintenance costs still have not been addressed. The following are our comments about the proposed system:

1. We have continually voiced our concerns about the open pond proposed by the developer. It has gone from a concrete water feature in early designs to a fabric lined pond in the current proposal. The open pond design increases maintenance costs and reduces the reliability of the system due to its susceptibility to debris, ice, moss, aquatic vegetation, and the substantial number of orchestrated parts that are need to make it work.
2. The developer has tried to mitigate some of these factors by doing two ponds with the first pond being a sediment pond to catch some of the debris before it flows into the pond with the pump intake. The creek system built into the subdivision that runs pretty little water ways may add to the ambiance of the neighborhood but does nothing but degrade the reliability of the fire protection system. If you want babbling brooks by all means put them in but don't tie them to a life safety system.
3. Ice will be a major factor and we cannot see on the plans how the system to keep the pond full during the winter months has addressed the icing questions we have voiced in the past. The first proposal and the only one we have seen had a simple surface mechanical float that would freeze in the ice and be nonfunctional unless some system was used to keep the water clear around the float. After repeated questions about how it would work, we still do not have an answer and there is nothing in this proposal that addresses the question. Unfortunately, we have to fight fire no matter the weather and this system must address how we get water out during extreme cold weather conditions and how the pond will automatically refill so it is ready for the next fire. They are still

guessing about how much ice will be on the surface of the pond. The pond has existed for at least two winters, why are they still guessing? Why wasn't the ice measured already?

4. The screen on the intake for the pump must be easily cleanable. It will plug and hiring a scuba diver to clean it each time is not practical, in our opinion. The cleaning method needs to be practical from the surface.
5. Also, in their proposal, they talk about chemically treating a pond in the middle of a subdivision designed for families. We are concerned about the toxicity of the water treatment, the durability of the liner, the ongoing cost of the maintenance, who is going to do the maintenance, the density of the inner circle not allowing enough space for the cranes, backhoes, draglines, etc. needed to perform maintenance.
6. The congested area in the center area makes tender operations, in the event of a water system failure, all but impossible providing for adequate safety.

Bottom line – this proposed fire water system is poorly thought out, completely ignores longevity and maintenance issues, was conceived around a constantly changing water feature which may enhance lot sales and aesthetic values but severely degrades the reliability of a fire water delivery system where reliability is paramount. The lives of our firefighters are dependent on the delivery of that water and with lot sizes of 0.18 acres, so are the lives housed in those homes built on lots 66 through lot 109. These lot sizes are representative of an urban setting without the benefit of a multimillion dollar water main and hydrant system to protect it. Fire spreading from structure to structure is a very real possibility with lot sizes of 0.18 acres. We request the current design be rejected and that a system built around reliability be required.

We believe a system with the pumps and controls currently proposed attached to an underground tank built on the space provided by the parking area and lots 90 and 109 would provide the reliability required and minimize the ongoing maintenance costs. The underground tank eliminates the reliability questions and ongoing maintenance relating to icing, sediment, chemicals, pond liners, pump screens, and access for maintenance.

We certainly realize the cost of an enclosed underground tank is not inconsequential. We have subdivisions currently with only 40 lots in them with underground tanks similar to what would be required for Heron Creek's 100+ lots. In our opinion the finite upfront costs measured in dollars of an underground tank are far less than the ongoing maintenance costs and reliability issues surrounding the developers proposal which will not only be measured in dollars passed on to the unsuspecting residents but may also be paid in lives when the system does not deliver when needed.

"Lewis and Clark County has a fiduciary responsibility to ensure fire danger is mitigated. At this time an effective and efficient means to mitigate fire dangers has not been reviewed due to recent decision by Judge Sherlock of Montana First Judicial District Court, Cause No. BVD-2005-418. The Applicant and Lewis and Clark County must agree, prior to final plat approval, on fire protection measures that minimize the risk of fire and that permit the effective and efficient suppression of fires."

Page 3

The proposed system does not provide an effective and efficient means to mitigate fire dangers and we, Tri-Lakes Fire Service Area, will not be fiduciarilly responsible for saying it does.

Sincerely,

TRI-LAKE VOLUNTEER FIRE DEPARTMENT

A handwritten signature in blue ink, appearing to read "Robert J. Drake", with a long horizontal flourish extending to the right.

Robert J. Drake, Fire Chief



Tri-Lakes Volunteer Fire Department

3200 Spokane Creek Road
East Helena, MT 59635

Phone & Fax: 406.475.3552

January 11, 2012

Greg McNally
L&C County Planning
316 N. Park Ave
Helena, MT 59623

Dear Greg:

The purpose of this letter is to provide comments on the proposed modification of approval for the Heron Creek Subdivision dated December 15, 2011.

There are several changes being requested that are interrelated from a public safety perspective and are addressed in the following comments:

1. We have dealt with several large subdivisions in the past that rolled out development in a phased approach to make the economics work. We are not opposed to the phased approach to this subdivision provided the proposed water system that is described in the attached letter from the engineering firm is installed and fully functional in PHASE I. The economics that are driving many of the changes also increase the risk that the subdivision may never be finished. The first home built has an expectation that promised fire protection infrastructure will be there to protect their family and property.
2. The water supply for the fire hydrants is described in the attached letter. In every discussion we have had with the developer and the engineer we have voiced our experience and our concern over the open design of the water supply. The engineer has drawn several modifications to reduce the effect of silt, surface litter, and ice from performance of the water system, however, we continue to have serious concerns about the ongoing maintenance.

The designs that use surface water from ponds, lakes, etc. are maintenance intensive and fail at a higher rate than closed loop systems (i.e. underground tanks, wells, etc.) As outlined in point #3 in the engineer's letter dated May 9, 2007 "This project anticipates full time maintenance personnel for the community, therefore helping to ensure the fire fill station remain in good operational condition." What happens now that the condo units proposed in the center are now all signal family dwellings? How are the "full time maintenance personnel" funded now?

Ongoing maintenance of the fire suppression infrastructure cannot be left to chance. We request that a Rural Improvement District (RID) we required from the beginning to insure funding of ongoing maintenance of the fire protection systems including the "water feature" that stores the water and all associated systems that maintain the level of the water, ice management features, silt management, security, etc.

3. The reconfiguration of the center to single family residences and the variance request to remove the requirement of utility easements drastically increases the fire safety concerns compared to the previous design. Proposed lot sizes of 0.16 acres or 6,922 sq. ft. forces the houses so close together that a fire could easily spread from house to house to house. The utility easements at least force space between the houses to reduce this risk. This reconfiguration makes these houses so dense that they are even smaller than some of the smallest lots in Helena. As proud as I am of our volunteer fire department, we do not compare to the City of Helena's Fire Department with six firefighters sitting at the stations waiting for an alarm. We provide protection with volunteers that have to respond from wherever they are when the emergency happens. Given our longer response times, available equipment, distance to travel, etc., we do not believe we can reasonably provide protection for the people who will live in these houses. We are absolutely OPPOSED to this density of structures given our level of capability. We are OPPOSED to the variance request for the removal of utility easements.
4. In the original design of this subdivision we had significant concerns and several discussions about the congestion in the core section of the subdivision. With the reconfiguration of the green phase in the developer's map, we are once again concerned about the narrow road width proposed, the lack of short-term and long-term parking for the residents and their numerous cars, boats, campers, jet skis, snow mobiles, etc. People have to have a place to park and if they can't find a legal one, they will park on the street. This new design heightens our concern for access for fire trucks and ambulances in this congested area. Space for designated parking has to be provided for residents and visitors on the street or off the street or reasonable access cannot be assured.

We understand the pressure that the current economic times must be putting on developers of current subdivisions, however, public safety should not be what is sacrificed. We believe that it has been with the reconfiguration of the core of this subdivision. The plan proposes a density that we simply do not believe we can adequately support.

Sincerely,
TRI-LAKE VOLUNTEER FIRE DEPARTMENT

A handwritten signature in blue ink, reading "Robert J. Drake". The signature is fluid and cursive, with a long horizontal stroke extending to the right.

Robert J. Drake, Chief

FIRE CONDITION AGREEMENT

This AGREEMENT ("Agreement") is entered into by and between Ron Bartsch ("Developer"), whose address is 3130 Saddle Drive Suite 5, Helena Montana 59601 and Lewis & Clark County ("County"), a political subdivision of the State of Montana and a body politic and corporate, with its principal place of business located at 316 North Park, Helena, Montana 59601.

RECITALS

WHEREAS, the Developer obtained preliminary approval to divide the property, which is known as Lot A-1A Amended of the H.W. Smith Minor Subdivision otherwise known as the *Heron Creek* Subdivision, on September 18, 2007 with 27 conditions of approval;

WHEREAS, the Developer requested modifications to the preliminary plat and conditions of approval on two occasions and was granted modifications to the preliminary plat and conditions of approval on November 6, 2008 and February 28, 2012 by the Lewis and Clark Commission;

WHEREAS, the modifications granted on February 28, 2012 included a six phase preliminary plat and additional conditions for each phase;

WHEREAS, condition numbers 9 (Phase I), 7 (Phase II), 7 (Phase III), 7 (Phase IV), 7 (Phase V), and 7 (Phase VI) of that preliminary approval state that the Developer and County "must agree, prior to final site plan approval, on fire protection measures that minimize the risk of fire and that permit the effective and efficient suppression of fires"; and

WHEREAS, the Developer's representative, Ryan Casne P.E. with Casne and Associates, Inc., has submitted fire suppression plans and supplemental information for the Heron Creek Subdivision, Phases I-III, attached to this Agreement as Exhibit A, to demonstrate a plan for fire protection measures that minimize the risk of fire and that permit the effective and efficient suppression of fires;

WHEREAS, the Developer's representative, Ryan Casne P.E. has acknowledged that the fire suppression plans and supplemental information shown in Exhibit A are for all 6 phases of the Heron Creek Subdivision as shown on the preliminary plat, attached to this Agreement as Exhibit B;

NOW, THEREFORE, County and the Developer agree as follows:

AGREEMENT

1. Condition Satisfied. The Parties agree that the fire suppression plans shown in Exhibit A are adequate to minimize the risk of fire and will permit the effective and efficient suppression of fires in the subdivision. As a result, the Parties agree that condition numbers 9 (Phase I), 7 (Phase II), 7 (Phase III), 7 (Phase IV), 7 (Phase V), and 7 (Phase VI) of the County's subdivision approval has been satisfied.

2. Third Party Rights: No person or entity, who is not a party to this Agreement, shall have any right of action under this Agreement.
3. Scope: This Agreement constitutes the entire agreement between the parties and no statement, promise, or inducement not contained in this Agreement shall be binding on the parties.
4. Governing Law and Venue: This Agreement shall be construed under and governed by the laws of the State of Montana. In the event of litigation concerning this Agreement, venue is in the First Judicial District Court, Lewis & Clark County, State of Montana.
5. Severability: If any part, term or provision of this Agreement is held by the courts to be illegal, the illegality shall not affect the validity of any other part, term, or provision, and the rights of the parties shall be construed as if the illegal part, term, or provision were never part of the Agreement.

Date: _____

Date: _____

Andy Hunthausen, Chairman
Board of County Commissioners
Lewis and Clark County

Ron Bartsch, Developer

State of Montana

County of _____

ATTEST:

Paulette J. DeHart, Clerk and Recorder

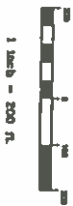
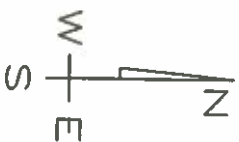
This instrument was acknowledged before
me on _____ by Ron Bartsch.

(Signature of notarial officer)

(Seal)

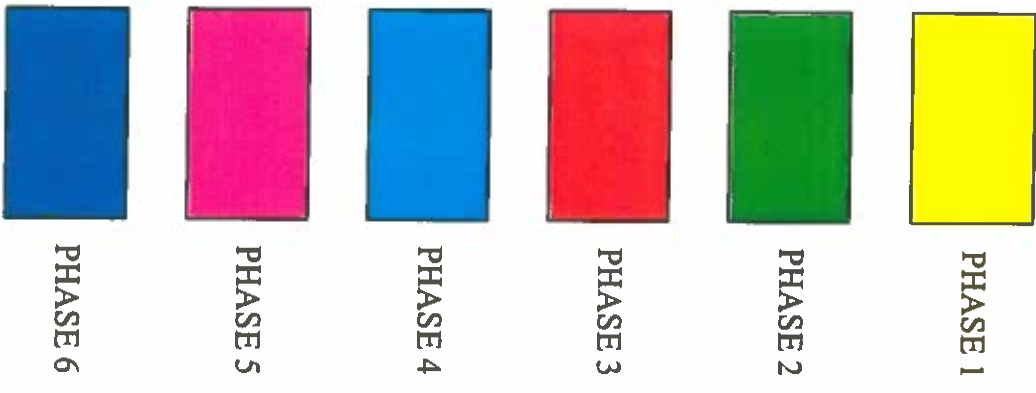
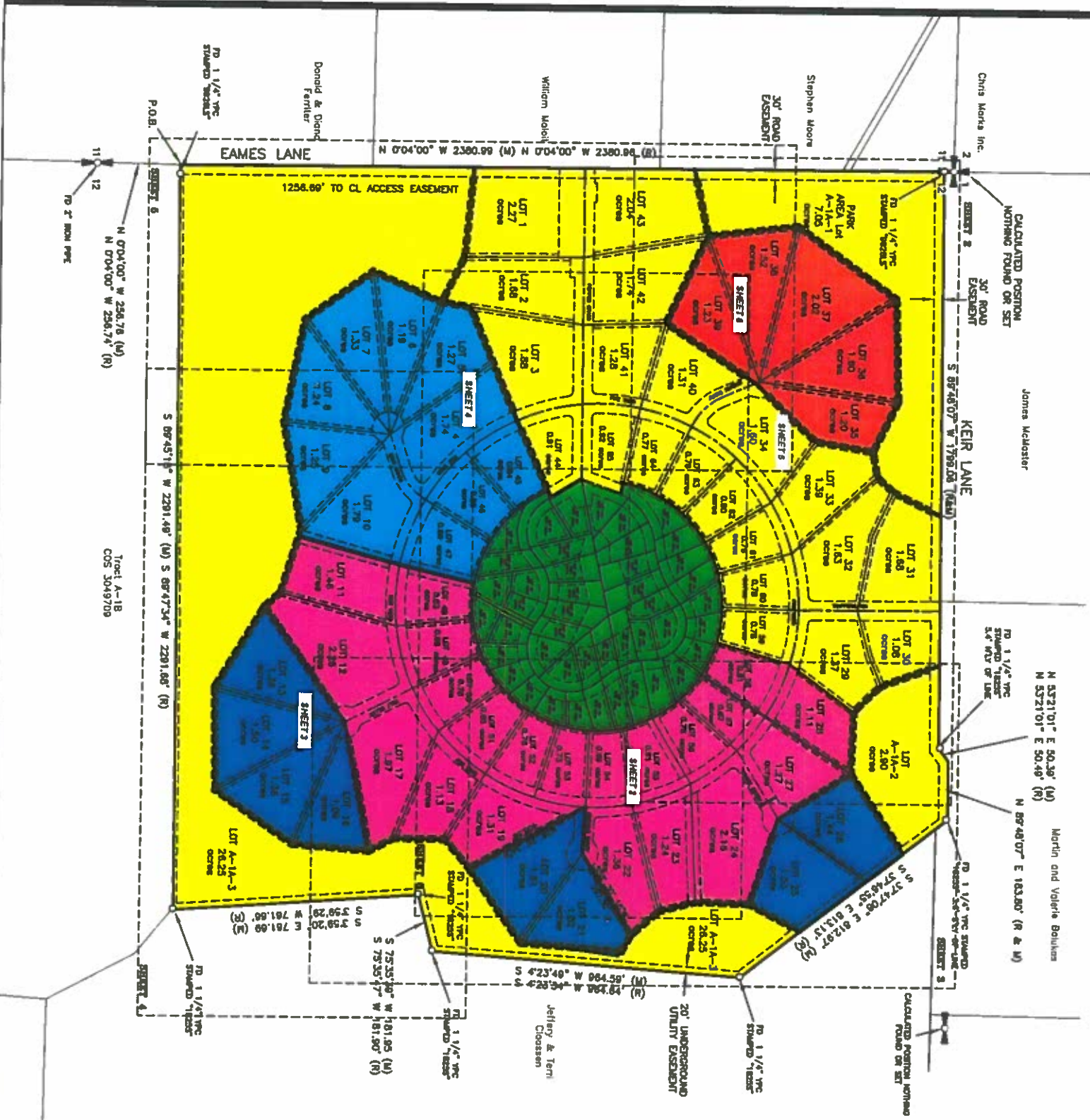
(Seal)

Approved as to form and content
(Deputy County Attorney)

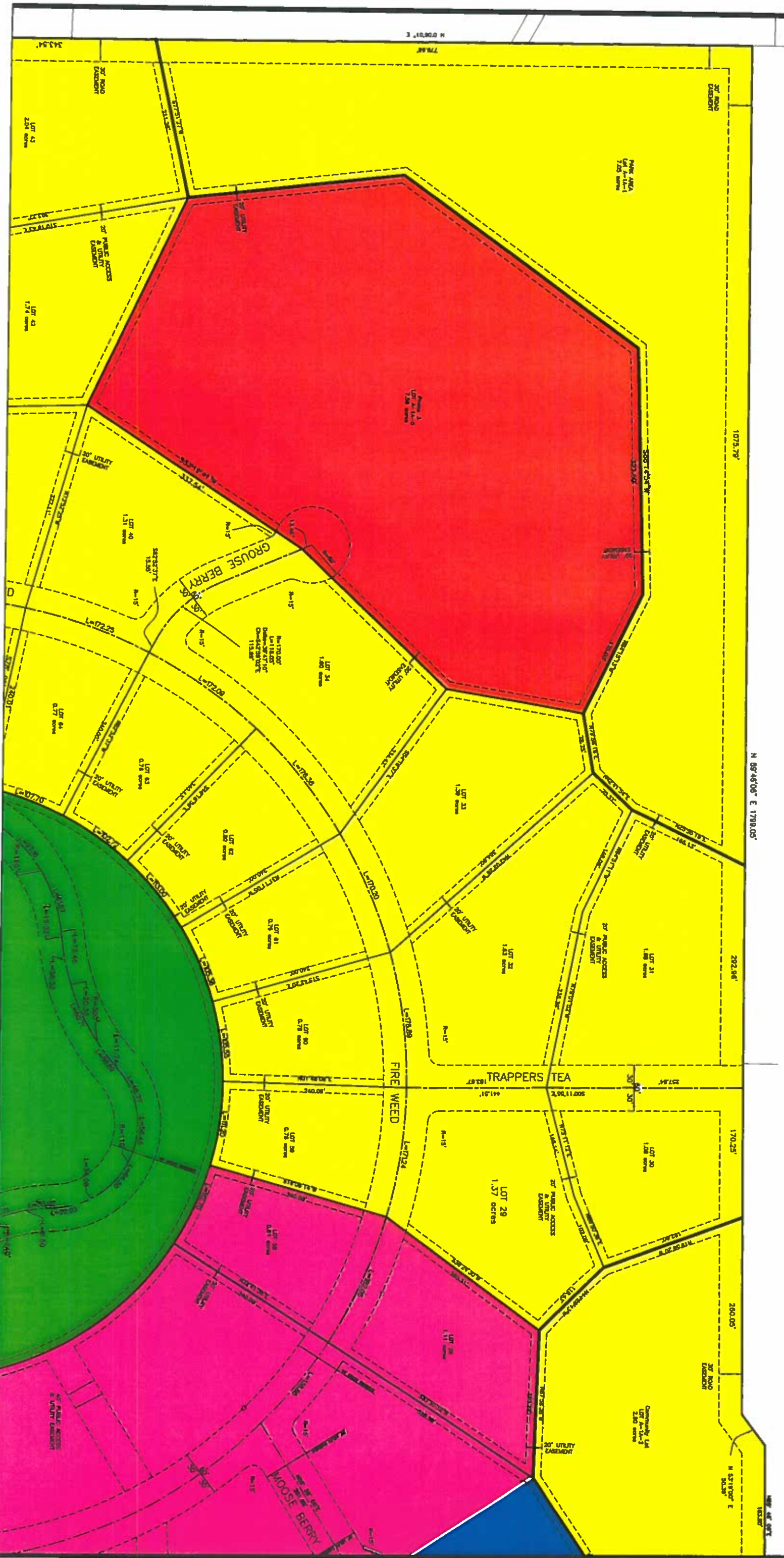


HERON CREEK SUBDIVISION, PRELIMINARY, ALL PHASES

BEING LOT A-1A, H.W. SMITH SUBDIVISION, COS 3049709
LOCATED WITHIN THE NORTHWEST 1/4 OF SECTION 12 T. 10 N., R. 2 W., P.M.M.
LEWIS & CLARK COUNTY, MONTANA
SHEET 1 of 12



<u>DESCRIPTIVE DATA</u>	
28	Number of Lots
129.62	Total acres being reviewed
36.20	Acres in Park/Common Facilities
4.64	Acres in Road Easements
0.76	Acres Minimum Lot size
33.06	Acres Maximum Lot Size



HERON CREEK SUBDIVISION, PRELIMINARY PLAT

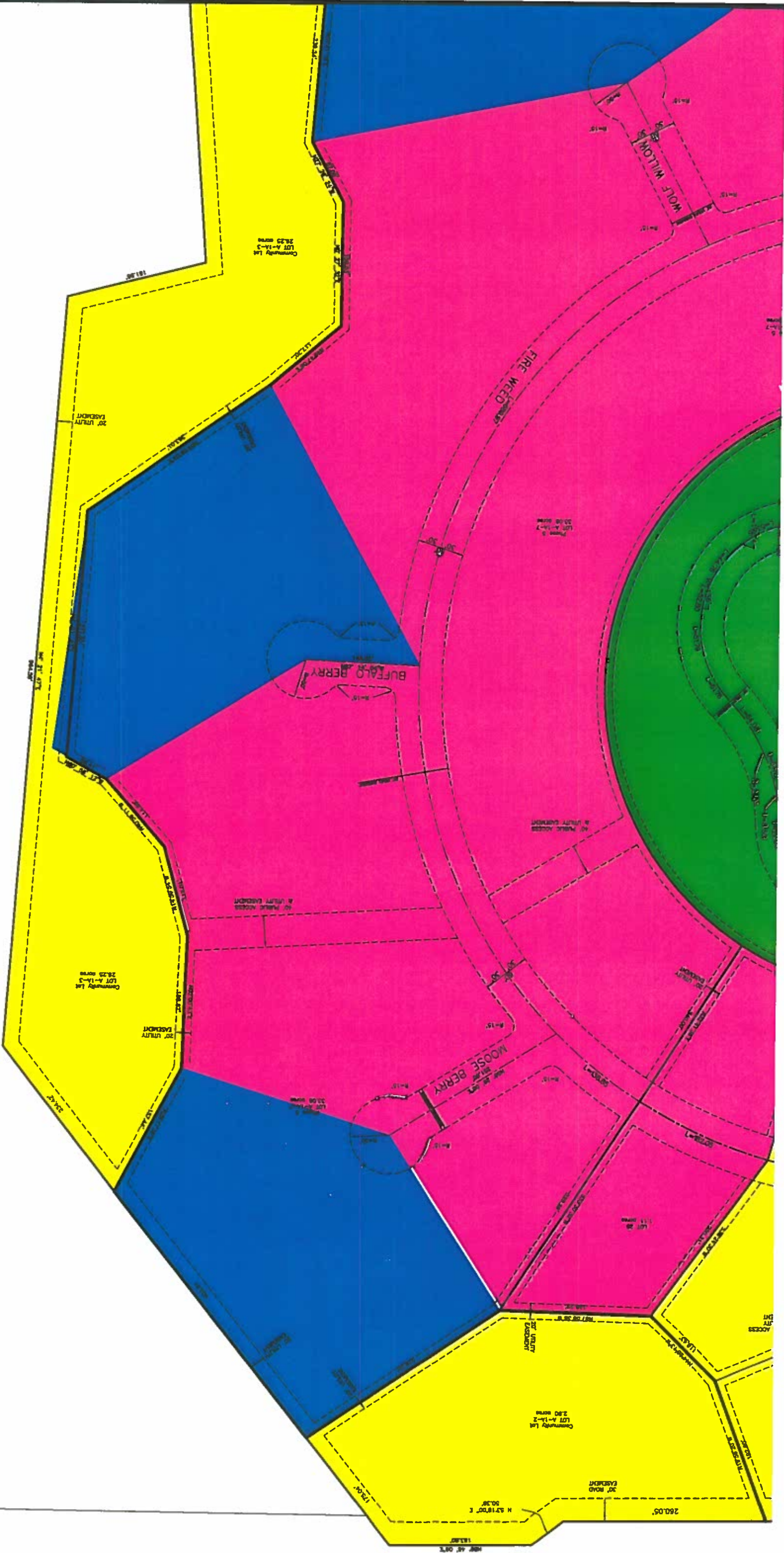
PHASE 1

BEING TRACT A-1A COS 3049709

LOCATED WITHIN THE NORTHWEST 1/4 OF SECTION 12 T. 10 N., R. 2 W., P.M.M.

LEWIS & CLARK COUNTY, MONTANA

SHEET 3 of 12



HERON CREEK SUBDIVISION, PRELIMINARY PLAT

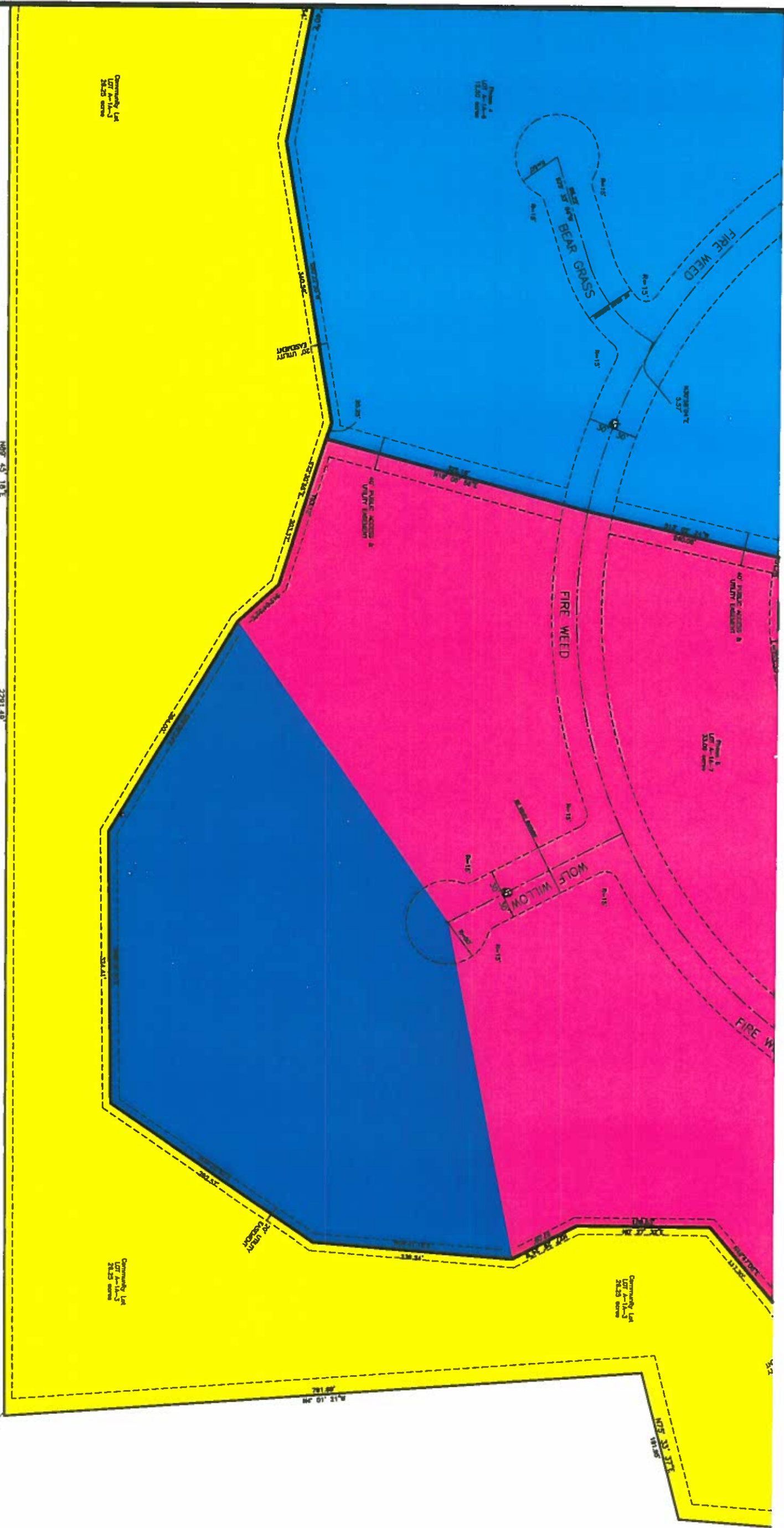
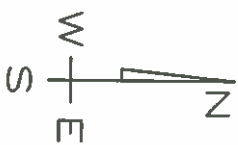
PHASE 1

BEING TRACT A-1A COS 3049709

LOCATED WITHIN THE NORTHWEST 1/4 OF SECTION 12 T. 10 N., R. 2 W., P.M.M.

LEWIS & CLARK COUNTY, MONTANA

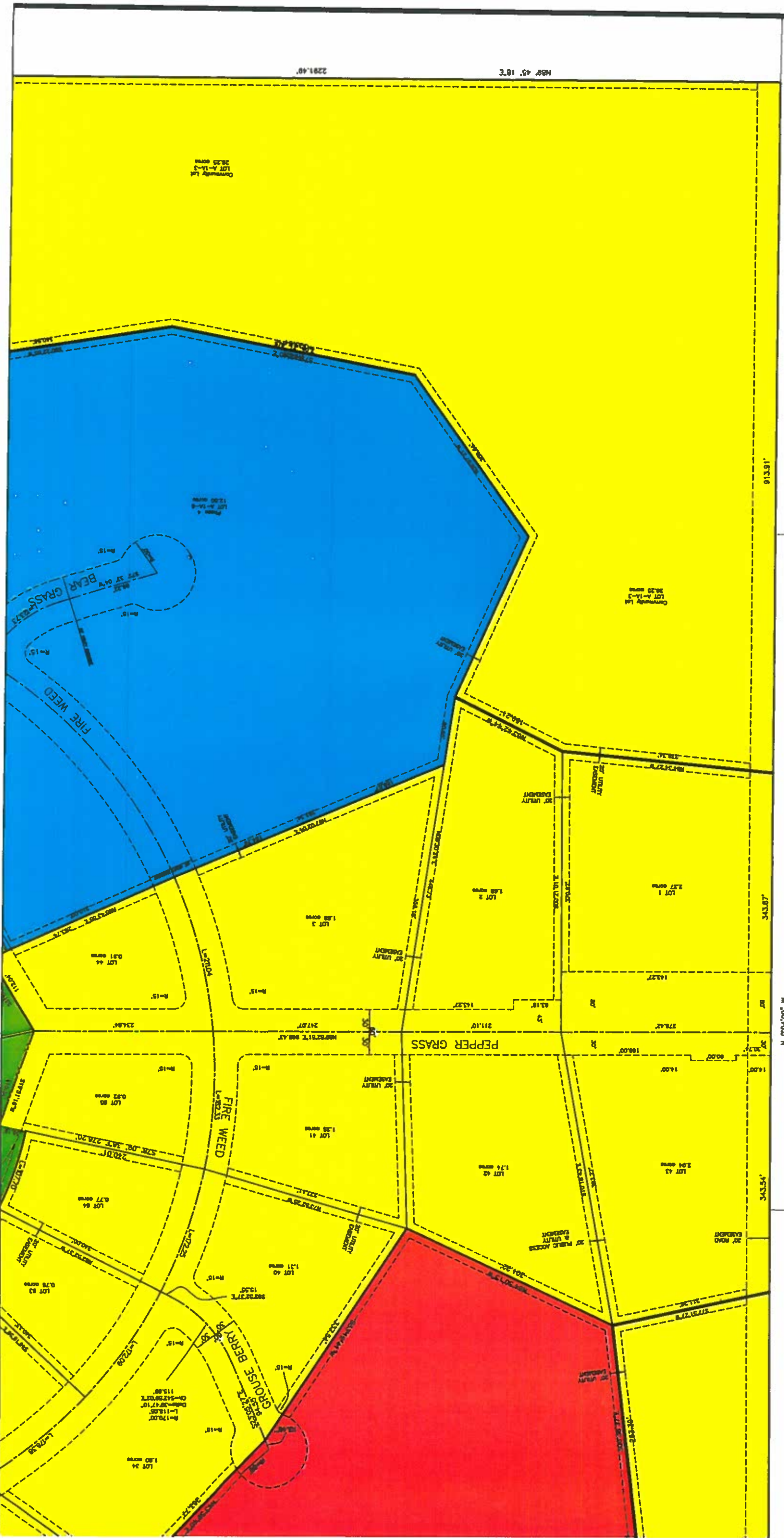
SHEET 4 of 12

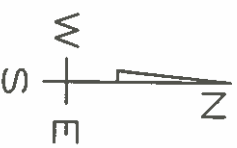




HERON CREEK SUBDIVISION, PRELIMINARY PLAT PHASE 1

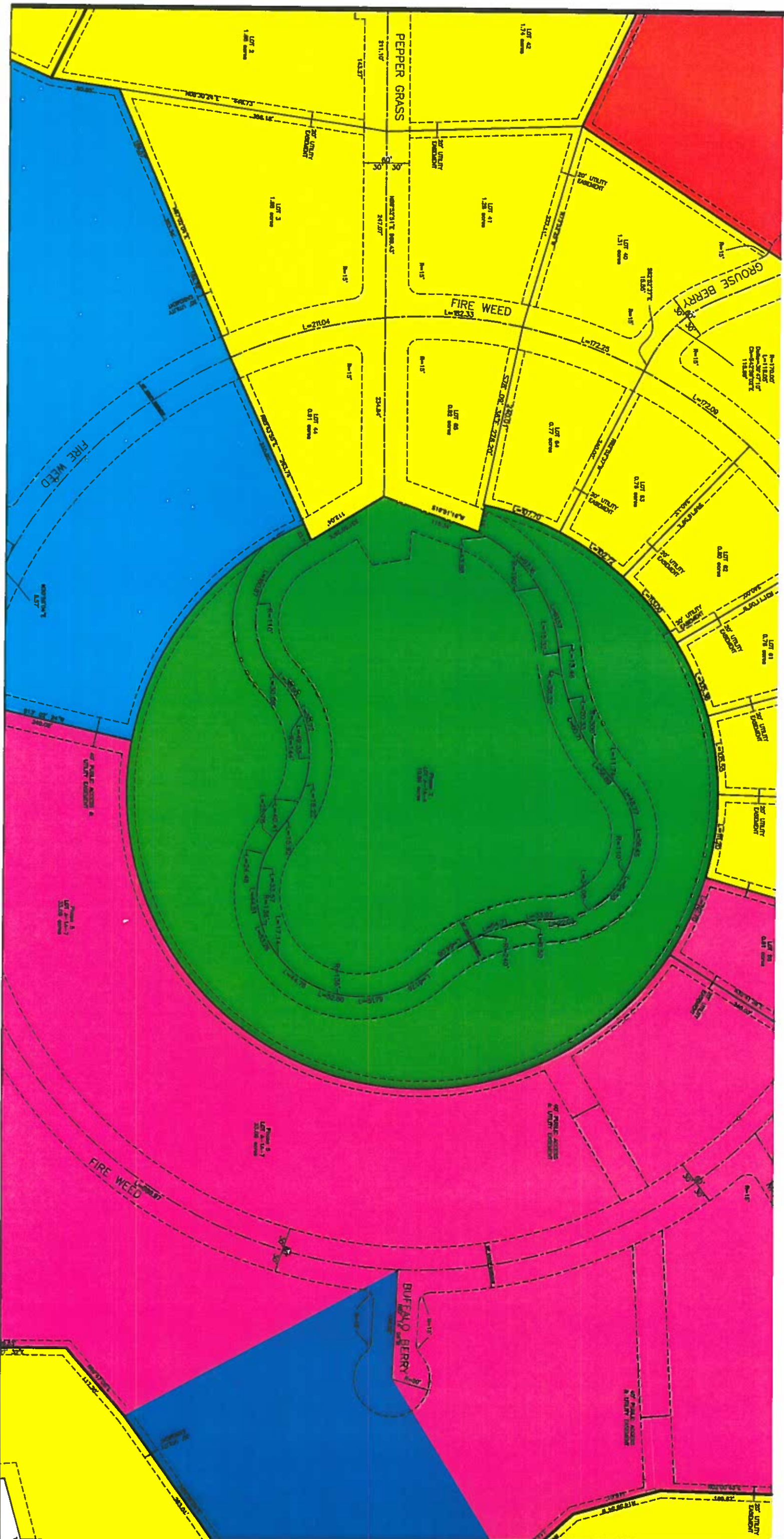
BEING TRACT A-1A COS 3049709
LOCATED WITHIN THE NORTHWEST 1/4 OF SECTION 12 T. 10 N., R. 2 W., P.M.M.
LEWIS & CLARK COUNTY, MONTANA
SHEET 5 of 12





HERON CREEK SUBDIVISION, PRELIMINARY PLAT PHASE 1

BEING TRACT A-1A COS 3049709
LOCATED WITHIN THE NORTHWEST 1/4 OF SECTION 12 T. 10 N., R. 2 W., P.M.M.
LEWIS & CLARK COUNTY, MONTANA
SHEET 6 of 12



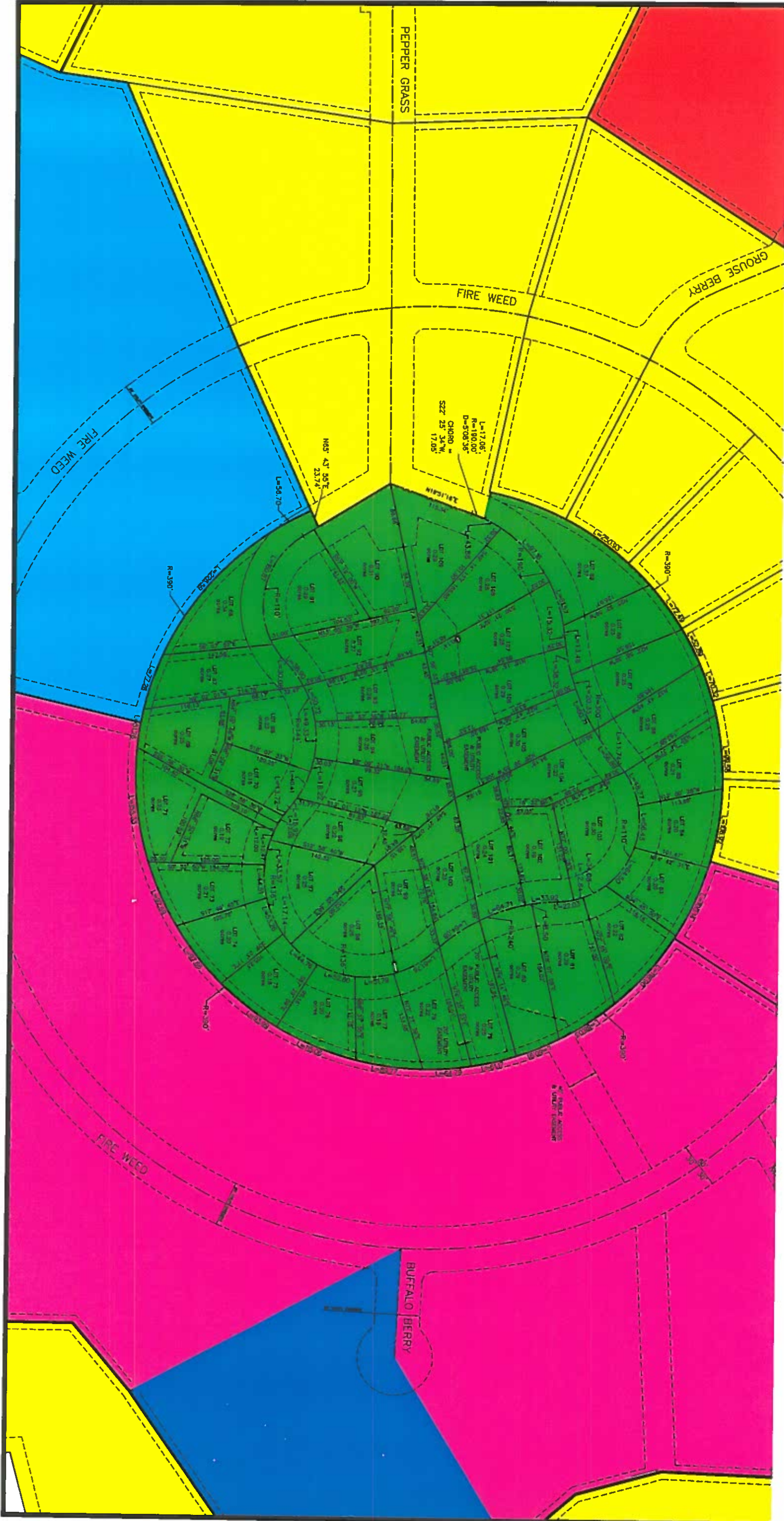
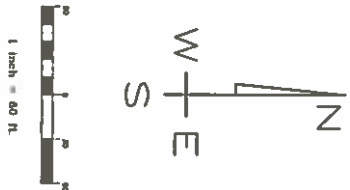
HERON CREEK SUBDIVISION, PHASE 2
PRELIMINARY

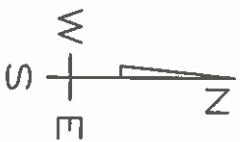
BEING TRACT A-1A-4, H.W. SMITH MINOR SUBDIVISION
LOCATED WITHIN THE NORTHWEST 1/4 OF SECTION 12 T. 10 N., R. 2 W., P.M.M.
LEWIS & CLARK COUNTY, MONTANA

SHEET 7 of 12

DESCRIPTIVE DATA

44	Number of Lots
10.87	Total acres being reviewed
0	Acres in Park/Common Facilities
2.43	Acres in Road Easements
0.16	Acres Minimum Lot size
0.37	Acres Maximum Lot Size



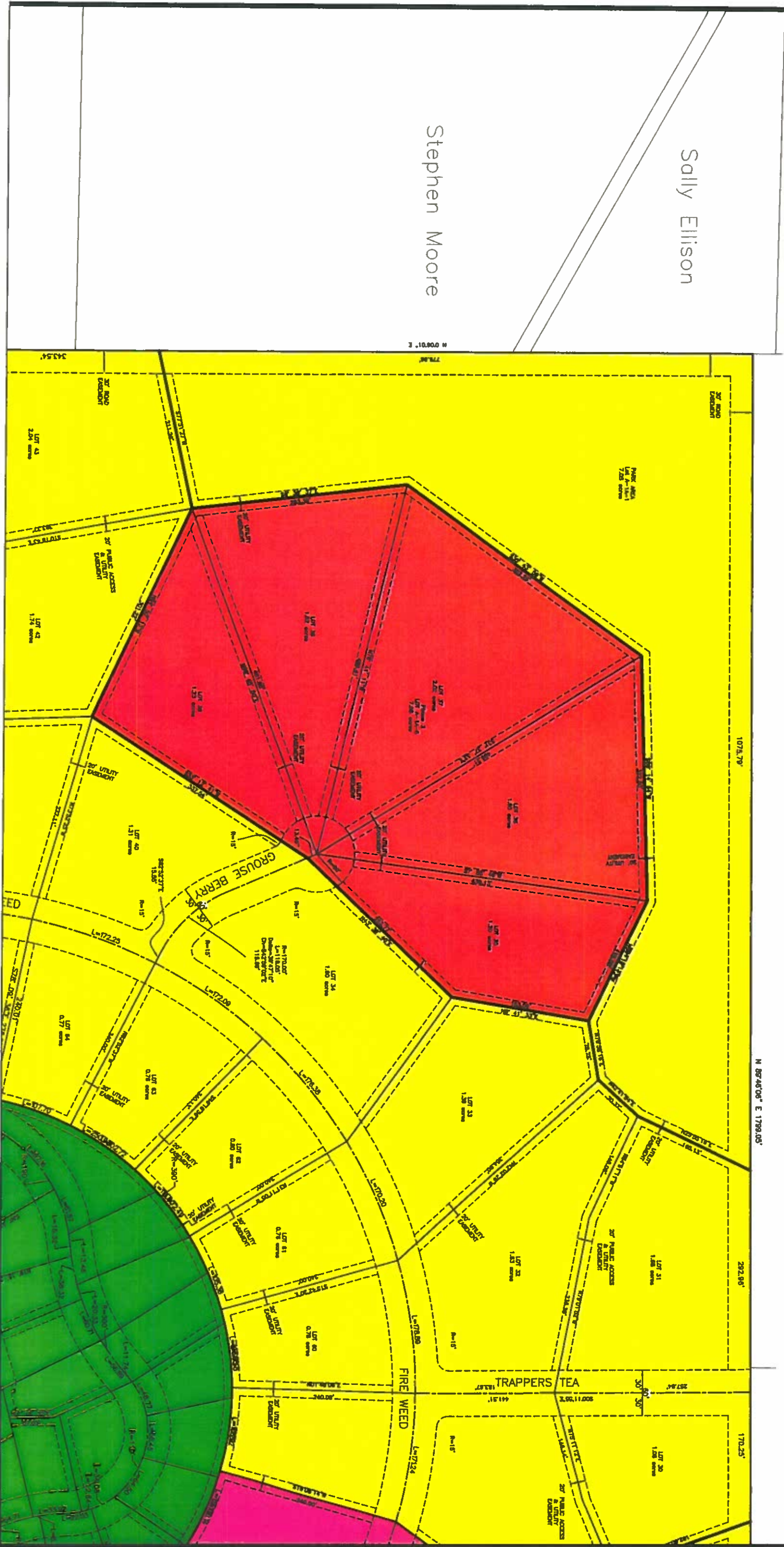


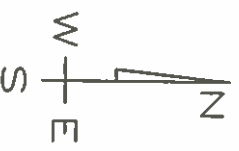
HERON CREEK SUBDIVISION, PHASE 3

PRELIMINARY

BEING TRACT A-1A-5 H.W. SMITH MINOR SUBDIVISION
LOCATED WITHIN THE NORTHWEST 1/4 OF SECTION 12 T. 10 N., R. 2 W., P.M.M.
LEWIS & CLARK COUNTY, MONTANA
SHEET 8 of 12

DESCRIPTIVE DATA	
Number of Lots	5
Total acres being reviewed	7.57
Acres in Park/Common Facilities	0
Acres in Road Easements	0
Acres Minimum Lot size	1.20
Acres Maximum Lot Size	2.02





HERON CREEK SUBDIVISION, PHASE 4

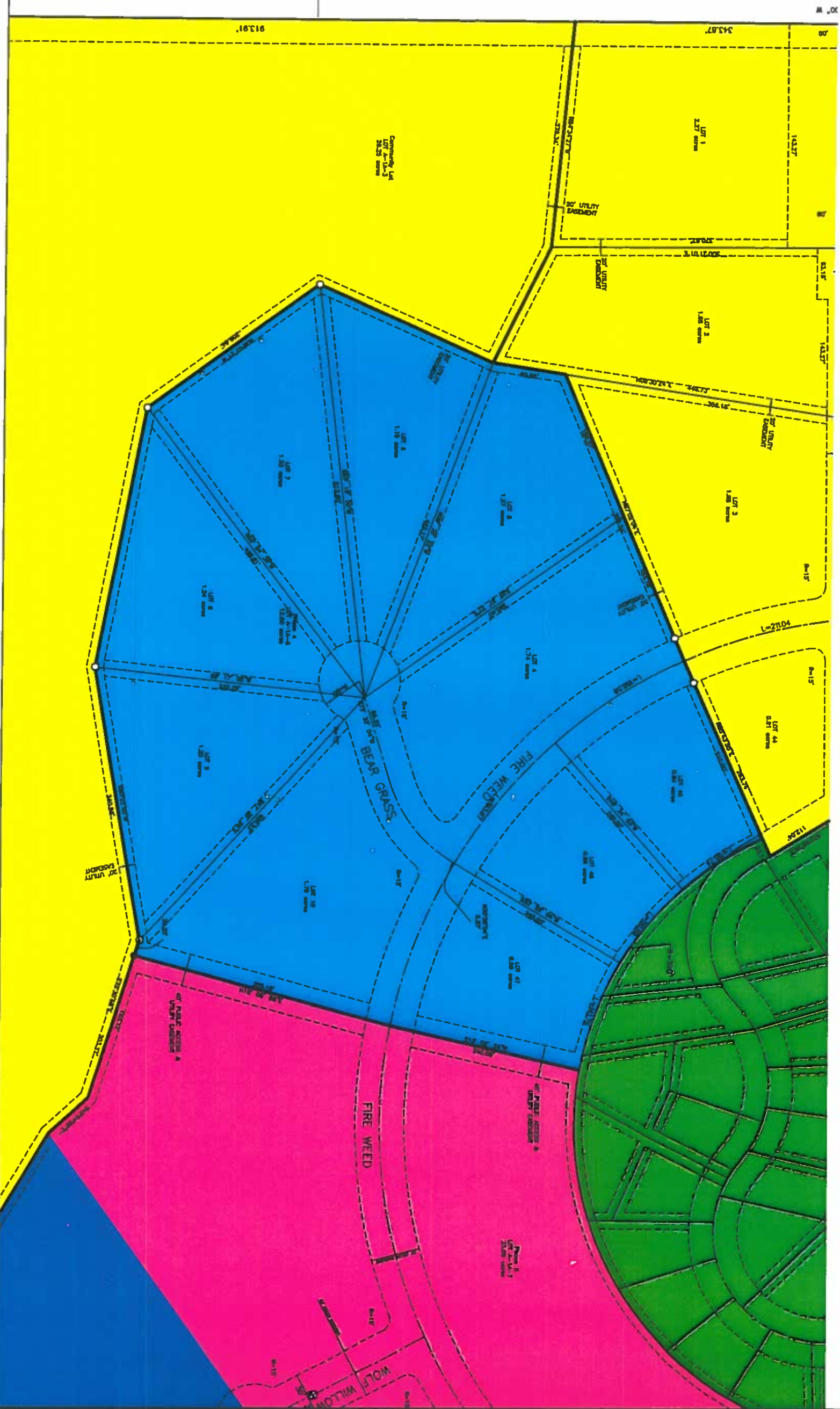
PRELIMINARY

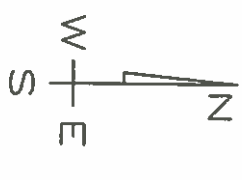
BEING TRACT A-1A -6 H. W. SMITH MINOR SUBDIVISION
LOCATED WITHIN THE NORTHWEST 1/4 OF SECTION 12 T. 10 N., R. 2 W., P.M.M.
LEWIS & CLARK COUNTY, MONTANA
SHEET 9 of 12

DESCRIPTIVE DATA	
10	Number of Lots
12.5	Total acres being reviewed
0	Acres in Park/Common Facilities
1.26	Acres in Road Easements
0.84	Acres Minimum Lot size
1.79	Acres Maximum Lot Size

Donald & Diana
Ferrier

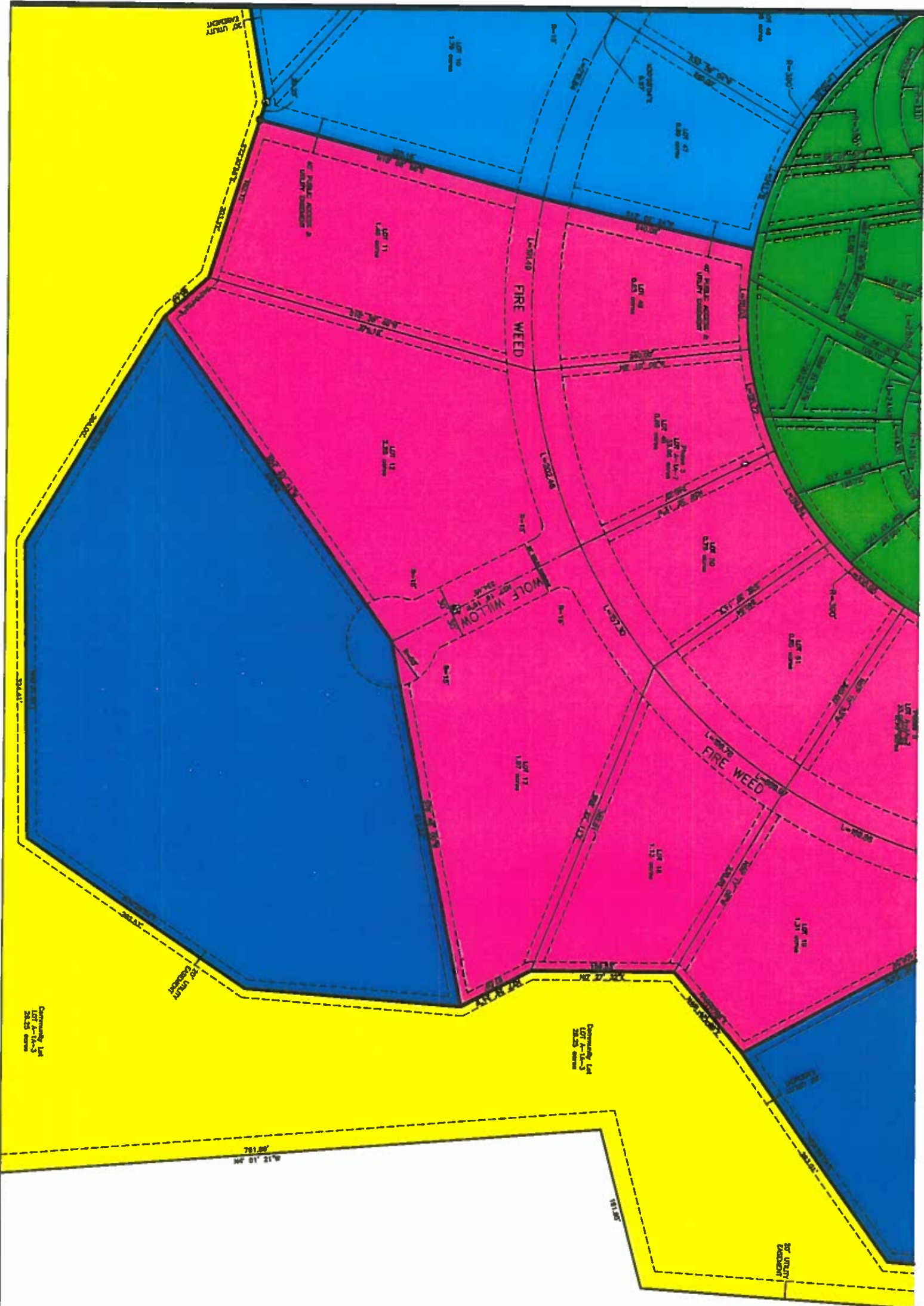
William Maloit





HERON CREEK SUBDIVISION, PHASE 5 PRELIMINARY

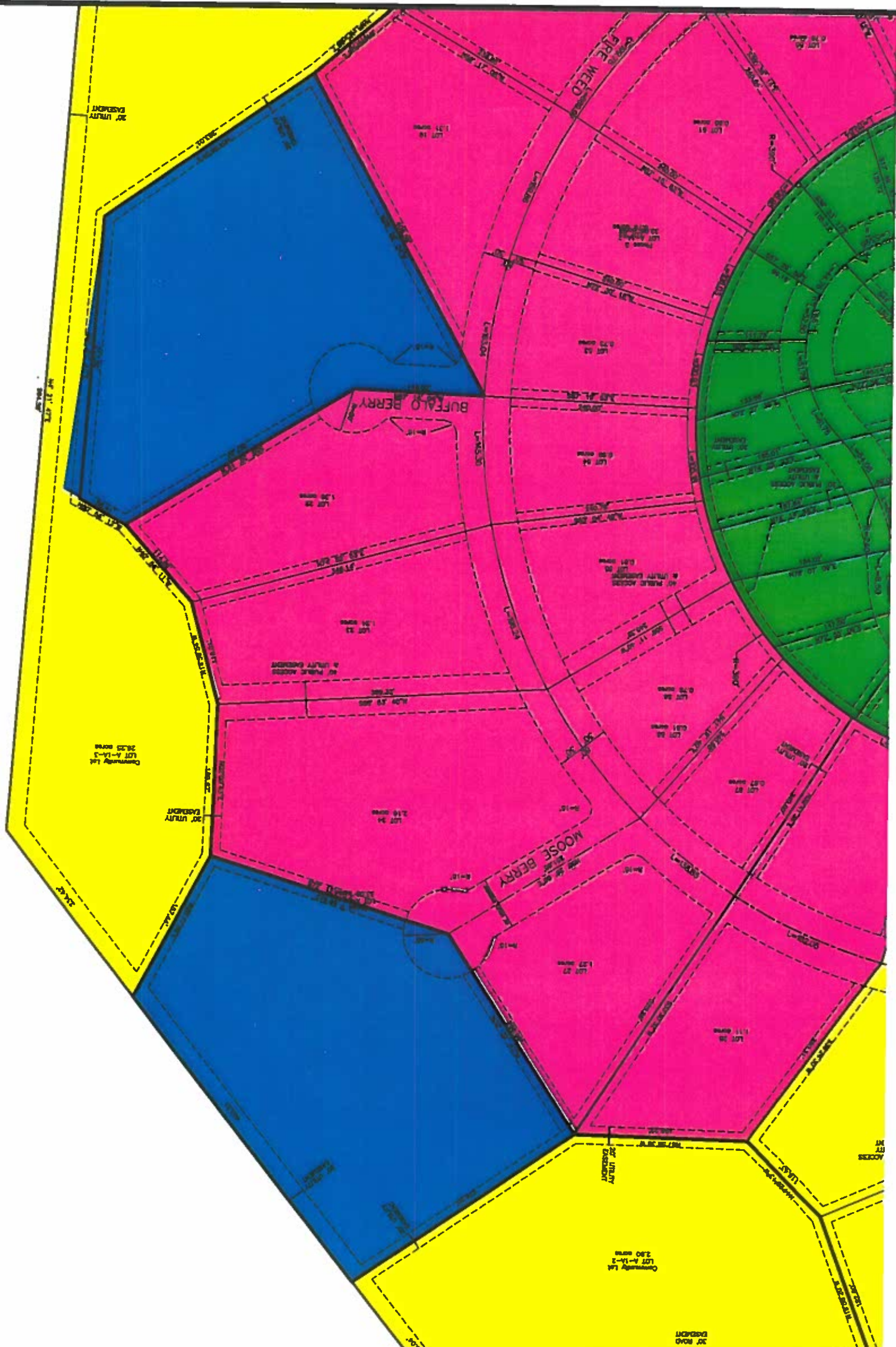
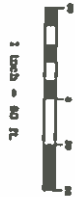
BEING TRACT A-1A-7, H. W. SMITH MINOR SUBDIVISION
LOCATED WITHIN THE NORTHWEST 1/4 OF SECTION 12 T. 10 N., R. 2 W., P.M.M.
LEWIS & CLARK COUNTY, MONTANA
SHEET 10 of 12

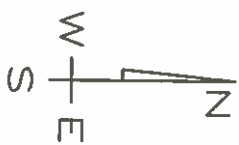


DESCRIPTIVE DATA	
24	Number of Lots
24.88	Total acres being reviewed
0	Acres in Park/Common Facilities
3.75	Acres in Road Easements
0.67	Minimum Lot size
5.31	Maximum Lot Size

HERON CREEK SUBDIVISION, PHASE 5
PRELIMINARY

BEING TRACT A-1A-7, H. W. SMITH MINOR SUBDIVISION
LOCATED WITHIN THE NORTHWEST 1/4 OF SECTION 12 T. 10 N., R. 2 W., P.M.M.
LEWIS & CLARK COUNTY, MONTANA
SHEET 11 of 12





HERON CREEK SUBDIVISION, PHASE 6 PRELIMINARY

BEING TRACT A-1A-7A, A-1A-7B, & A-1A-7CH.W. SMITH MINOR SUBDIVISION
LOCATED WITHIN THE NORTHWEST 1/4 OF SECTION 12 T. 10 N., R. 2 W., P.M.M.

LEWIS & CLARK COUNTY, MONTANA

SHEET 12 of 12

DESCRIPTIVE DATA	
Number of Lots	8
Total acres being reviewed	11.21
Acres in Park/Common Facilities	0
Acres in Road Easements	0
Acres Minimum Lot size	1.09
Acres Maximum Lot Size	1.53

